

11 YORKVILLE PARTNERSHIP INC.

# 11-21 YORKVILLE AVENUE FUNCTIONAL SERVICING REPORT -

MARCH 23, 2018





# 11 YORKVILLE AVENUE FUNCTIONAL SERVICING REPORT - DRAFT

11 YORKVILLE PARTNERSHIP INC.

FUNCTIONAL SERVICING REPORT - DRAFT

PROJECT NO.: 17M-01494

DATE: MARCH 23, 2018

WSP CANADA GROUP LIMITED  
100 COMMERCE VALLEY DRIVE WEST  
THORNHILL, ON, CANADA L3T 0A1

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## **APPENDICES**

- A** THEORETICAL SANITARY SEWAGE FLOWS & SANITARY DESIGN SHEETS & SANITARY DRAINAGE AREA PLAN (SDR-1)
- B** DOMESTIC WATER DEMAND, HYDRANT FLOW TESTING RESULTS AND FUS FIRE FLOW CALCULATIONS
- C** CITY OF TORONTO DORSCH MODEL SHEETS & SEWER ATLAS MAPS

# 1 INTRODUCTION

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## 1.1 SCOPE OF MUNICIPAL SERVICING

WSP Canada Group Limited (WSP) has been retained by 11 Yorkville Partnership Inc. to prepare a Functional Servicing Report (FSR) in support of the proposed development of 11-21 Yorkville Avenue and 16-18 Cumberland Street in the City of Toronto (herein referred to as Buildings A and B, respectively, or 'site'). The site is located on the south side of Yorkville Avenue just west of Yonge Street and on the north side of Cumberland just west of Yonge Street. The total site area is approximately 0.32 ha. As shown in Figures 1 and 2, the site is bound by Yorkville Avenue to the north, city-owned laneways to the south and east and a 71-storey building (pre-construction) to the west. It is assumed that the existing buildings are serviced by existing infrastructure in the municipal right-of-way (ROW). The purpose of this report is to outline how water, sanitary and storm servicing will be provided for the redevelopment of the site.

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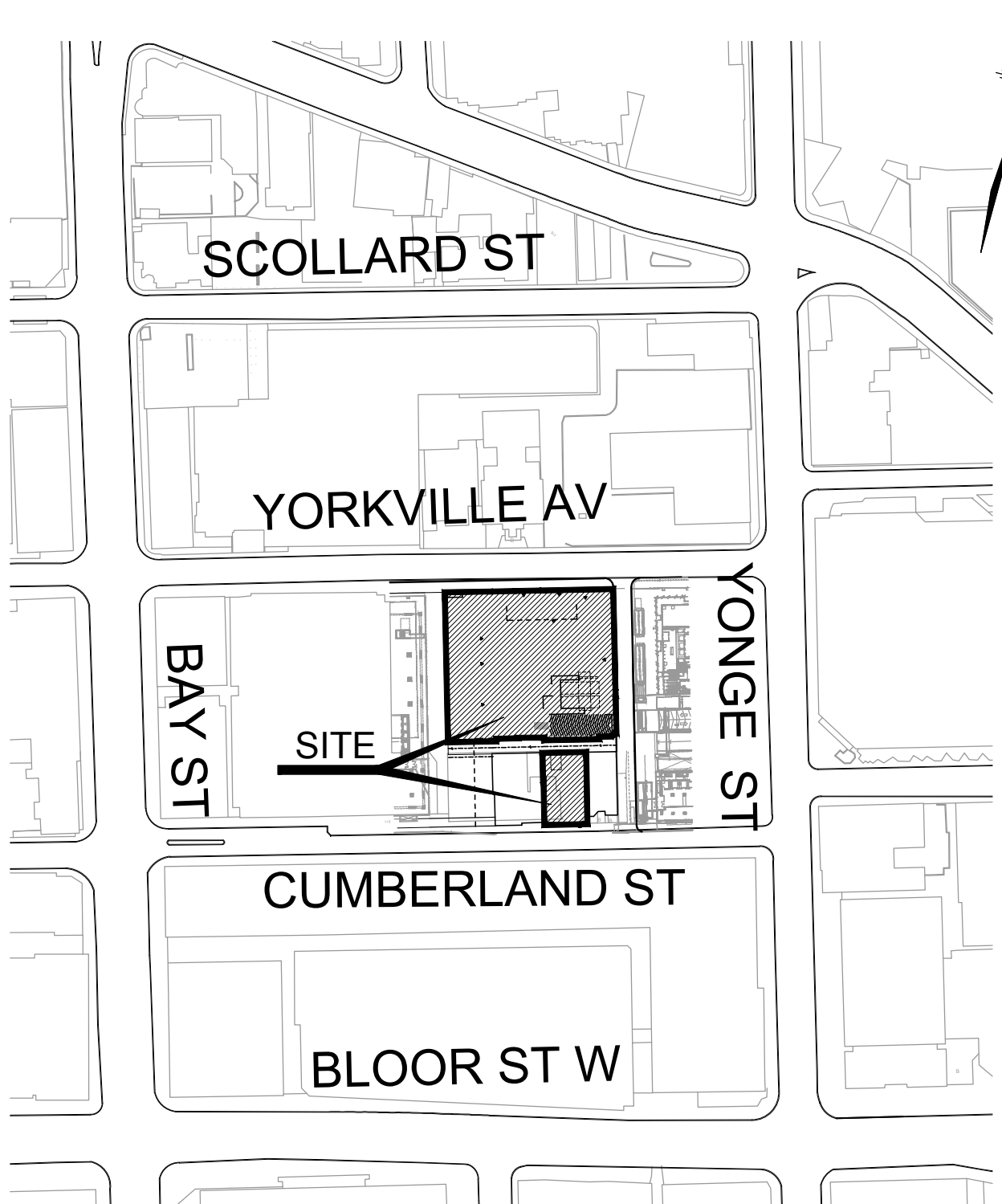
## 1.2 EXISTING CONDITIONS


Currently, 11 Yorkville Avenue is occupied by a 10-storey commercial building with an underground parking structure at its rear. 17 Yorkville Avenue is occupied by a three-storey commercial building with a small backyard area. 19 Yorkville Avenue and 21 Yorkville are both occupied by four-storey commercial buildings. 16 Cumberland Street is occupied by a four-storey commercial building and 18 Cumberland Street is occupied by a two-storey commercial building. We have assumed that all existing buildings have existing services to the municipal sewers. Please refer to Figure 2 for the Pre-Development Plan.

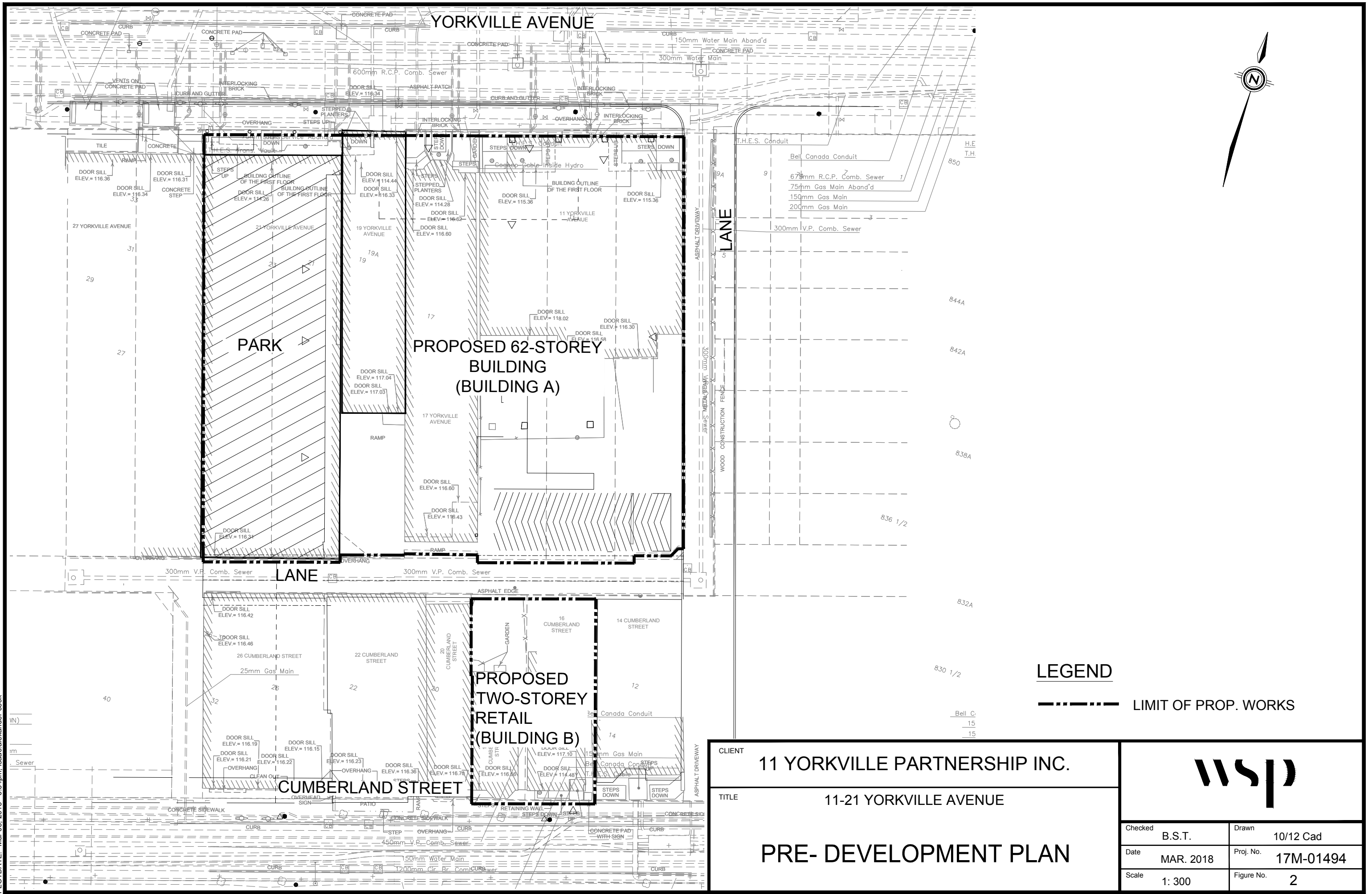
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## 1.3 PROPOSED DEVELOPMENT

The proposed development consists of one 62-storey mixed-use tower (Building A) and one two-storey retail (Building B). Building A will have four (4) below-grade parking levels, 716 residential units and approximately 3,818 m<sup>2</sup> of retail space. Privately-Owned Public Space (POPS) and park area will be located west of Building A. Building B will have one below-grade concourse level and two above-ground levels, with a total of 846 m<sup>2</sup> of retail space. All service connections for Building A will be provided from existing infrastructure on Yorkville Avenue and for Building B, service connections will be directed to both Cumberland Street and the laneway on the north side. All vehicle access to Building A will be provided by an entrance at the north east corner of the site that will run along the east side of the site and pass underneath the building to reach the underground parking entrance. Please refer to Figure 3 for the Proposed Development Plan.

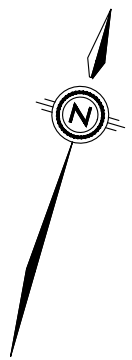
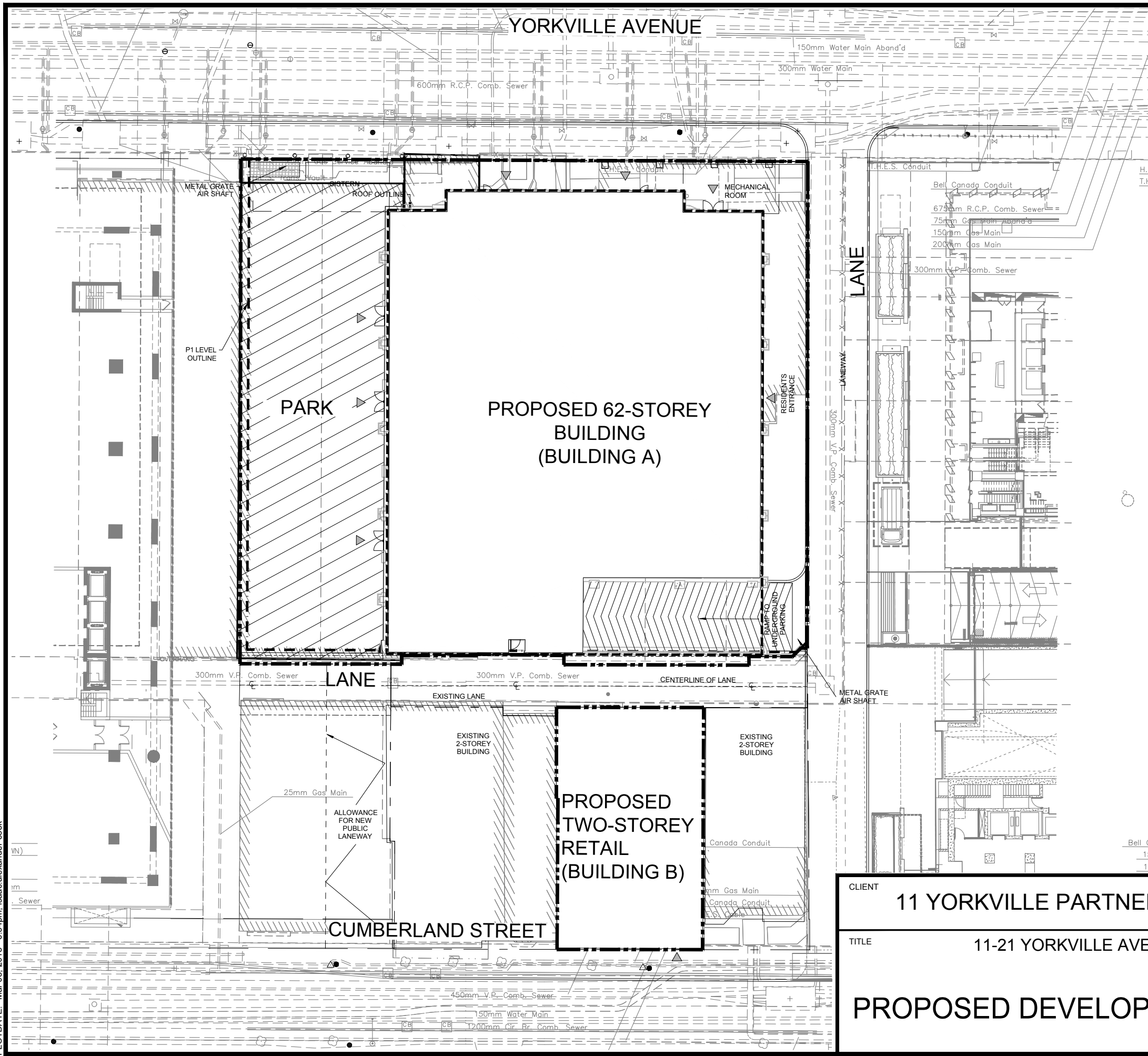


CLIENT 11 YORKVILLE PARTNERSHIP INC.		
TITLE 11-21 YORKVILLE AVENUE  <b>LOCATION PLAN</b>		
	Date MAR. 2018	Proj. No. 17M-01494
	Scale NTS	Figure No. 1



PLOT DATE: Mar 08, 2018 - 6:54pm - isaac.alexander-cook





**LEGEND**

- LIMIT OF PROP. WORKS
- ROOF OUTLINE
- P1 LEVEL OUTLINE

CLIENT	11 YORKVILLE PARTNERSHIP INC.
TITLE	11-21 YORKVILLE AVENUE
PROPOSED DEVELOPMENT PLAN	

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Date	Proj. No.
MAR. 2018	17M-01494
Scale	Figure No.
1: 300	3

PLOT DATE: Mar 08, 2018 - 6:54pm. isaac.alexander-cook

# 2 SANITARY SEWAGE SYSTEM

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## 2.1 EXISTING CONDITIONS

The existing sewers in the vicinity of the site are a 600 and 675 mm diameter V.P. combined sewer on Yorkville Avenue, and a 300 mm diameter V.P. combined sewer along the public lanes to the east and south of Building A, as shown on Figure 2. The 600 and 675 mm V.P. combined sewer on Yorkville Avenue flows east towards Yonge Street. The 300 mm diameter V.P. combined sewer in the public lane flows east, then north to join the combined sewer on Yorkville Avenue.

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## 2.2 DESIGN PARAMETERS

The following sanitary design criteria have been taken from City of Toronto, Design Criteria for Sewers and Watermain, November 2009:

- ▶ 450 L/cap/day average day flow generation rate for residential use (new development on an existing combined sewer system)
- ▶ 240 L/cap/day average day flow generation rate for existing residential use
- ▶ 250 L/cap/day average day flow generation rate for existing commercial use
- ▶ Population densities of 2.7 person per suite for existing apartment buildings;
- ▶ 1.4 people per single bedroom or studios, 2.1 people per two-bedroom unit and 3.1 people per three bedroom unit.
- ▶ Peaking Factor
  - Residential Harmon, Harmon Peaking Factor =  $1+14/(4+p^{0.5})$ , where p = population in thousands.
  - Institutional/Commercial (included in average flow)
- ▶ Infiltration = 0.26 L/s/ha

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## 2.3 EXISTING FLOWS TO THE SANITARY SEWER SYSTEM

Using the design criteria noted in Section 2.2, the sanitary flows from the existing buildings are calculated in Table 2.1:

**Table 2.1 – Existing Sanitary Flows to Yorkville Avenue**

Address	Gross Floor Area (GFA)	Site Area	Population	Average Commercial Flow (250 L/cap/d)	Infiltration Allowance (0.26 L/s/ha)	Total Existing Sanitary Flow
	(m <sup>2</sup> )	(ha)	(ppl)	(L/s)	(L/s)	(L/s)
11 Yorkville Avenue	7700	0.077	85	0.25	0.02	0.27
17 Yorkville Avenue	1158	0.039	13	0.04	0.01	0.05
19 Yorkville Avenue	1004	0.025	12	0.03	0.01	0.04
21 Yorkville Avenue	3140	0.079	35	0.10	0.02	0.12
16 Cumberland Street	828	0.021	10	0.03	0.01	0.03
18 Cumberland Street	477	0.016	6	0.02	0.00	0.02
<b>Total</b>	<b>14,307</b>	<b>0</b>	<b>161</b>	<b>0.47</b>	<b>0.07</b>	<b>0.53</b>

The total sanitary flow from the existing development was calculated to be 0.53 L/s.

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## 2.4 PROPOSED SANITARY FLOWS

The projected sanitary flows from the development have been estimated using the design criteria outlined in Table 2.2:

**Table 2.2 – Sanitary Design Criteria & Proposed Sanitary Flows to Yorkville Avenue**

Residential Sanitary Demand Rate	450 litres/person/day
Residential Population Density	1.4 people per studio and one bedroom units 2.1 people per two bedroom units 3.1 people per three bedroom units
Commercial Population Density	1.1 people per 100 m <sup>2</sup>
Residential units	716 units
Residential studio/1 bedroom units	426 units
Residential 2 bedroom units	218 units
Residential 3 bedroom units	72 units
Total Residential Population	1279 people
Total Commercial Population	42 people
Residential Peaking Factor	$1+14/(4+p^{0.5})$ , where p = population in thousands = 3.73
Commercial Peaking Factor	1.0 - Retail Peak is offset from Residential Peak – therefore Peak Flow = Peak Residential + Average Retail
Permanent Dewatering Rate	2.37 L/s
Average Res. Sanitary Flow from Site	6.66 L/s
Infiltration Allowance (0.26 L/s/ha)	0.08 L/s
Peak Residential Sanitary Flow from Site	24.84 L/s
Total Commercial Sanitary Flow	0.15 L/s
<b>Total Sanitary Flow from Site</b>	<b>27.44 L/s</b>
<b>Net increase in Flow (post - pre)</b>	<b>26.91 L/s</b>

Based on the calculated sanitary flows found in Table 2.2, the site will generate 27.44 L/s of sanitary flow. Building A will discharge to the existing 675 mm combined sewer along Yorkville Avenue through one 200 mm diameter residential sanitary service connection and one 100 mm diameter commercial sanitary connection. Building B will discharge flow to the existing 300 mm combined sewer in the laneway north of the building via a 100 mm diameter sanitary service connection. This combined sewer ultimately connects to the combined sewer on Yorkville Avenue. Sanitary control maintenance holes will be installed immediately inside the property line for both Buildings A and B, which will be accessible at all times to City staff. Installation of these connections will be coordinated with the City of Toronto connections department. All other internal plumbing will meet Ontario Building Code standards.

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## 2.5 ANALYSIS OF DOWNSTREAM COMBINED SEWERS

The City of Toronto has provided copies of the City’s Dorsch model data and Sewer Atlas Maps for the combined sewers on Yorkville Avenue, Yonge Street and the surrounding network of pipes. Those copies of the Dorsch model and Sewer Atlas Maps are provided in Appendix C and are only used as a reference to complete the design sheet for pre and post development. The design sheets and sanitary drainage area plan can be found in Appendix A.

A dry weather downstream sewer analysis was completed for the pre-development and post-development conditions. Pipe capacities remain below 5% in both the pre-development and post-development conditions. This demonstrates that the existing sewer system is capable of accommodating dry weather flow from the proposed development.

Since the theoretical flows from the proposed development do not negatively impact the existing sewer system as demonstrated in the post-development design sheets, WSP has concluded that the downstream sewer system is adequate for the proposed redevelopment and no downstream sewer improvements are required to service this development.

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## 2.6 COMPLIANCE WITH MOECC PROCEDURE F-5-5

It is proposed to discharge both sanitary and storm flows to the existing 675 mm combined sewer on Yorkville Avenue. MOECC procedure F-5-5 requires that the total flow in the combined sewer system not increase as a result of the proposed development.

**Table 2.3 – Comparison of Pre- and Post-Development discharge to combined sewer**

	Pre-Development Flow	Post-Development Flow	Net Change
Sanitary	0.5 L/s	27.4 L/s	26.9 L/s
Storm	72.5 L/s	31.9 L/s	-40.6 L/s
Total	73.0 L/s	59.3 L/s	<b>-13.7 L/s</b>

As shown in the table above, there is a net decrease of 13.7 L/s in the total flow draining to the existing combined sewer system as a result of the proposed development. Therefore, no capital improvements to the municipal combined sewer system are required since flow conditions in the existing combined sewer are improved in post-development.

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## 2.7 GROUNDWATER DISCHARGE

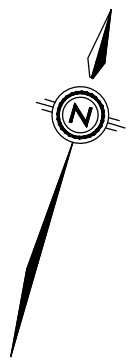
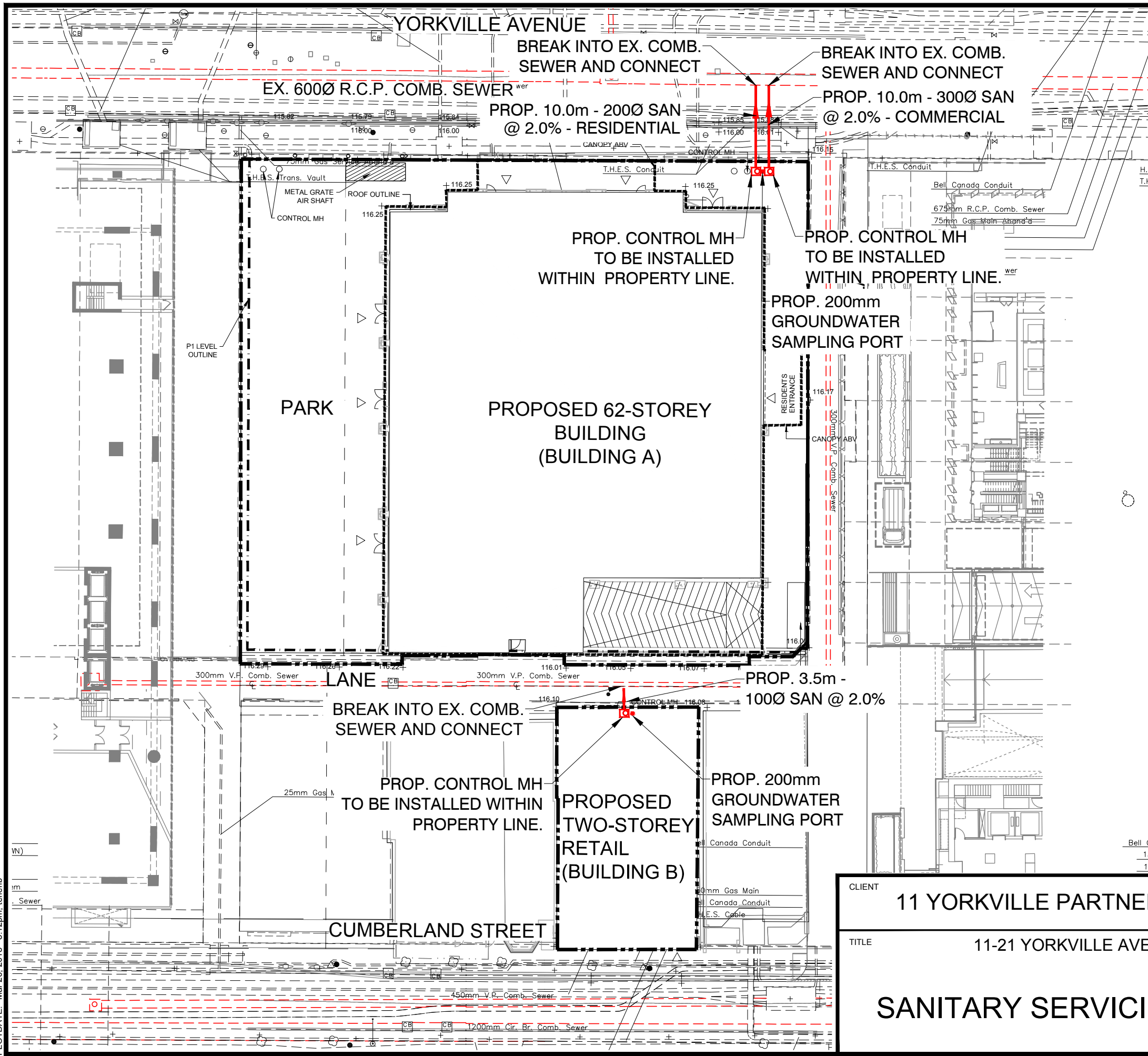
The client has retained the services of a hydrogeological specialist to study the discharge rate and quality of the foundation on the site and provide recommendations. A draft hydrogeological report was completed by EXP Services Inc. (EXP) on February, 28 2018 under a separate cover.

As stated in EXP's report, groundwater levels encountered in the monitoring wells at ground level ranged from approximately 3.19 to 3.40 meters below ground surface (mbgs). Shallow monitoring wells installed below ground revealed perched groundwater levels ranging from 0.44 mbgs to 5.33 mbgs, and deep monitoring wells revealed groundwater at depths ranging from 15.8 to 27.45 mbgs. The analytical results for the groundwater samples showed that the groundwater quality will meet the "Guidelines Limits for Sanitary & Combined Sewers Discharge" with the exception for Total Suspended Solids (TSS). This typically means that elevated concentrations of metals and inorganic parameters exceeding the Guideline Limits for Sanitary Sewer Discharge. Thus, groundwater will be discharged to the combined sewer.

As stated in the report, the total construction dewatering for the site is 286 m<sup>3</sup>/day or 3.31 L/s and the permanent foundation drainage rate for the site is 205 m<sup>3</sup>/day or 2.37 L/s to the combined sewer. The permanent foundation drainage rate of 2.37 L/s was added to the total sanitary flow calculation in Table 2.2 above and to the combined sewer analysis in Appendix A.

This additional flow to the sanitary system has been added to the external sanitary capacity analysis in Appendix A. As stated in the previous section, the capacity of the combined sewer does not exceed 5% full as a result of the proposed development. Based on this capacity, the external sanitary system can accommodate the additional groundwater rate.

Groundwater will be pumped to the bottom of the sanitary control manhole and then will flow by gravity into the municipal sewer. Sampling ports will be installed upstream of the control manholes and will be accessible from outside at any time, to allow City staff to monitor groundwater. This will ensure the water does not exceed the sanitary quality sewer discharge limits established by the City of Toronto.



**LEGEND**

- LIMIT OF PROP. WORKS
- ROOF OUTLINE
- P1 LEVEL OUTLINE
- EX. COMBINED SEWER
- PROP. SAN CONNECTION

CLIENT	<b>11 YORKVILLE PARTNERSHIP INC.</b>
TITLE	<b>11-21 YORKVILLE AVENUE</b>
<b>SANITARY SERVICING PLAN</b>	

Checked	B.S.T.	Drawn	10/12 Cad
Date	MAR. 2018	Proj. No.	17M-01494
Scale	1: 300	Figure No.	4

PLOTDATE: Mar 26, 2018 - 8:12pm. tefarib

# 3 WATER SUPPLY AND APPURTENANCES

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## 3.1 EXISTING CONDITIONS

Existing watermains in the vicinity of the site include a 300 mm watermain on Yorkville Avenue and a 150 mm watermain on Cumberland Street. There is an existing fire hydrant on the north-west corner of Yorkville Avenue and Yonge Street.

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## 3.2 DESIGN PARAMETERS

The following sanitary design criteria have been taken from the City of Toronto, Design Criteria for Sewers and Watermain, November 2009:

- ▶ Water demand rate of 191 L/person/day for proposed developments;
  - ▶ Population densities of 1.4 person per unit for one bedroom units;
  - ▶ Population densities of 1.4 person per unit for studio units;
  - ▶ Population densities of 2.1 person per unit for two bedroom units;
  - ▶ Population densities of 3.1 person per unit for three bedroom units;
  - ▶ Population densities of 2.7 person per unit for existing apartment buildings;
  - ▶ Peak Hour Factor of Residential = 2.48;
  - ▶ Maximum Day Factor of Residential = 1.65;
  - ▶ Peak Hour Factor of Commercial = 1.20;
  - ▶ Maximum Day Factor of Commercial = 1.10;
  - ▶ Retail Equivalent Population of 1.1 people / 100m<sup>2</sup> per floor space;
- 

## 3.3 DOMESTIC WATER DEMAND

The domestic water demands for the proposed development were calculated using the criteria's outlined by the City of Toronto's, design criteria for sewers and watermains, November 2009. The projected water demands for the proposed development have been estimated in Table 3.1:



**Table 3.1 – Design Criteria and Projected Domestic Water Demands from Site**

Average Water Consumption Rate	191 litres/person/day
Residential 1 Bedroom Unit & Population Density	426 units / 1.4 people per unit
Residential 2 Bedroom Unit & Population Density	218 units / 2.1 people per unit
Residential 3 Bedroom Unit & Population Density	72 units / 3.1 people per unit
Total Residential Units – Building A	716 units
Total Residential Equivalent Population – Building A	1279 people
Commercial Floor Area – Building A	3818 m <sup>2</sup>
Commercial Floor Area – Building B	846 m <sup>2</sup>
Commercial Population Density	1.1 people per 100 m <sup>2</sup> of floor area
Total Commercial Equivalent Population – Building A	42 people
Total Commercial Equivalent Population – Building B	10 people
Peaking Factors	Residential = 2.50 for Peak Hour, 1.30 for Maximum Day Commercial = 1.20 for Peak Hour, 1.10 for Maximum Day
Average Water Demand - Building A	2.92 L/s
Average Water Demand - Building B	0.02 L/s
Peak Water Demands - Building A	<b>Peak Hour = 7.18 L/s, Maximum Day = 3.78 L/s</b>
Peak Water Demands - Building B	<b>Peak Hour = 0.03 L/s, Maximum Day = 0.02 L/s</b>
Peak Water Demands – Site	<b>Peak Hour = 7.21 L/s, Maximum Day = 3.81 L/s</b>

The average day water demand for Building A will be 2.92 L/s and the average day demand for Building B will be 0.02 L/s. The peak hour and maximum day water demands are 7.18 L/s and 3.78 L/s for Building A and 0.03 L/s and 0.02 L/s for Building B, respectively. Please refer to Appendix B for detailed calculations of the domestic water demands.

### 3.4 PROPOSED WATER SERVICE

For Building A, the proposed water service connections will include two (2) 200 mm diameter fire lines each with one (1) 150 mm domestic branch connecting into the north side of the building from the existing 300 mm diameter watermain along Yorkville Avenue. Two separate fire connections separated by a valve and box will satisfy section 3.29.7(4) of the Ontario Building Code, which requires two separate fire connections for buildings exceeding 84.0m in height. The westerly 150 mm branch will supply residential flow while the easterly 150 mm branch will supply commercial flow. Building B will be serviced by one (1) 150 mm shared water line at the south side of the building which will connect to the existing 150 mm watermain on Cumberland Street. In accordance with City standards, water meters and detector check valves will be installed as close to the property line as possible for all domestic connections, and will be accessible from inside the buildings. All other internal plumbing will meet O.B.C. standards.

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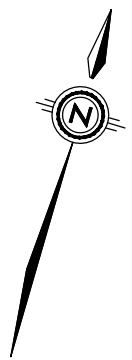
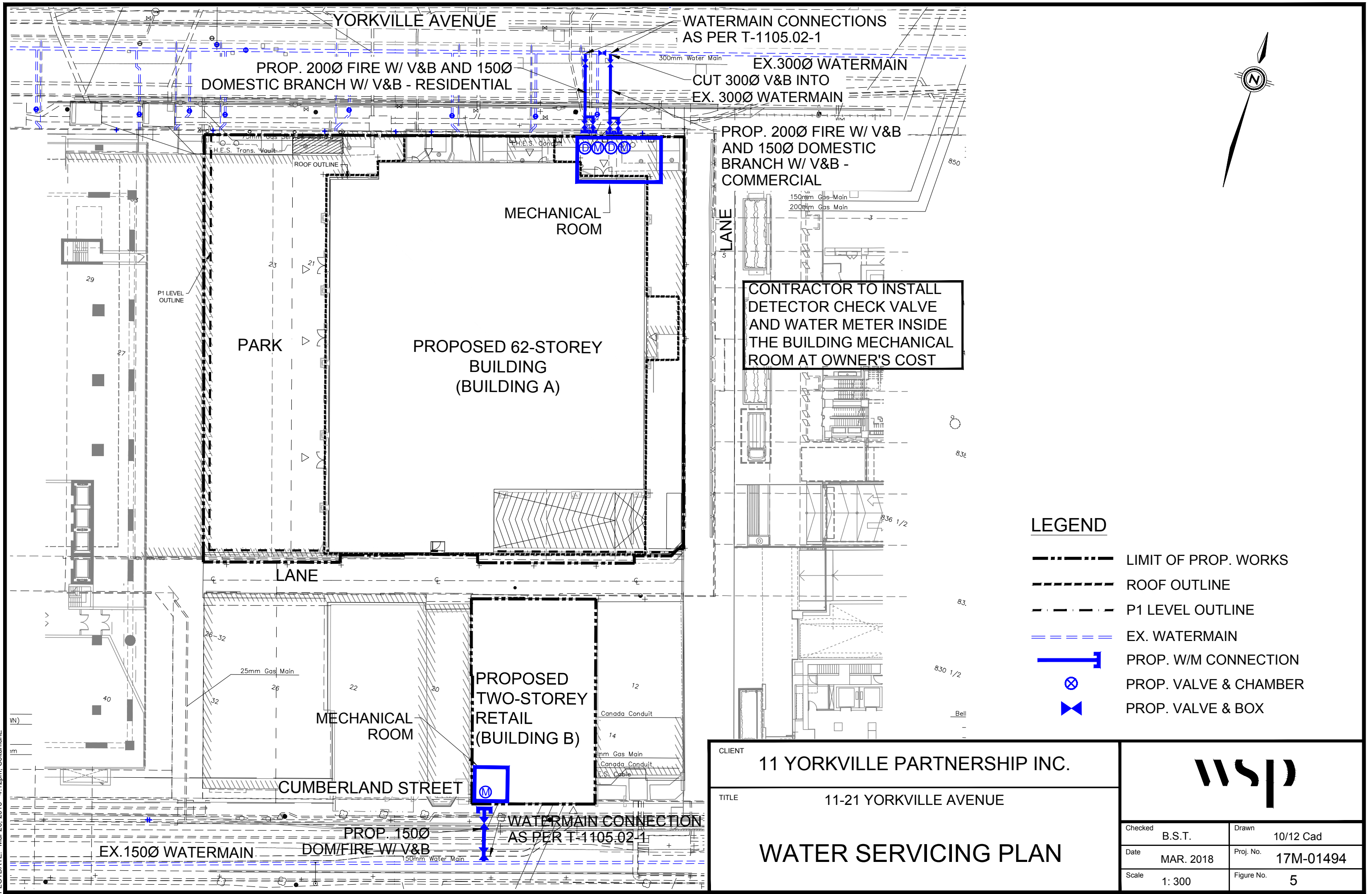
## 3.5 HYDRANT FLOW TEST

The required fire flow for the site was calculated based on the Fire Underwriters Survey (FUS) requirements. The calculations are based on the largest floor area, in addition to 25% of the floor area above, and 25% of the floor area below as the proposed building will be fire-resistive with vertical openings being adequately protected for a one hour fire. The required fire flow calculations are shown in Appendix A and are summarized in Table 3.2 below:

**Table 3.2– FUS Fire Flow for Proposed Development**

Site	Required Fire Flow (L/s)	
	USGPM	L/s
Building A	1801	114
Building B	920	58

Due to the winter season, hydrant flow testing has not yet been completed for the proposed development. Once the testing season re-opens after April, hydrant flow tests will be scheduled on both the existing 300 mm watermain on Yorkville Avenue and the existing 150 mm diameter watermain on Cumberland Street to assess the available capacity of the systems. The results of the hydrant flow tests will be compared with the calculated maximum day plus fire demands of the proposed Buildings A and B.



CONTRACTOR TO INSTALL  
 DETECTOR CHECK VALVE  
 AND WATER METER INSIDE  
 THE BUILDING MECHANICAL  
 ROOM AT OWNER'S COST

**LEGEND**

- LIMIT OF PROP. WORKS
- ROOF OUTLINE
- P1 LEVEL OUTLINE
- EX. WATERMAIN
- PROP. W/M CONNECTION
- PROP. VALVE & CHAMBER
- PROP. VALVE & BOX

CLIENT	11 YORKVILLE PARTNERSHIP INC.	
TITLE	11-21 YORKVILLE AVENUE	
	<b>WATER SERVICING PLAN</b>	
Checked	B.S.T.	Drawn 10/12 Cad
Date	MAR. 2018	Proj. No. 17M-01494
Scale	1: 300	Figure No. 5

PLOT DATE: Mar 26, 2018 - 4:12pm, SoltanianE

# 4 STORM DRAINAGE AND STORM DRAINAGE

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## 4.1 EXISTING CONDITIONS

The existing site is currently occupied by commercial buildings, covering the majority of the site. Since the runoff coefficient from the existing site exceeds 0.50, a runoff coefficient of 0.50 was used in the pre-development condition to determine the allowable release rate to the municipal storm sewers. Based on the site area of 0.323 ha and the 2-year rainfall intensity of 88.2 mm/hour (for a time of concentration of 10 minutes), the allowable 2-year pre-development release rate from the proposed development was calculated to be 39.6 L/s (35.2 L/s for Building A and 4.4 L/s for Building B). The existing site is estimated to have a current runoff coefficient of 0.90 with an existing storm flow rate of 72.5 L/s. Based on the existing topographic information, there are no external flows entering the site in its existing condition.

---

## 4.2 PROPOSED DEVELOPMENT

Building A and Building B will each have proposed stormwater cisterns which will collect stormwater runoff generated from the proposed site. A sump will be provided to detain stormwater to be irrigation, car washing, or toilet flushing of commercial spaces.

The City's WWFMG state that the maximum allowable discharge to a municipal sewer system is the 2-year pre-development flow rate for events of up to and including 100-year intensity. Based on this requirement, the cisterns will be sized to retain the water captured onsite during a 100-year storm and release at the 2-year pre-development rate to the proposed 200 mm storm service connection which will direct flow to the existing 600 mm diameter combined sewer on Yorkville Avenue (Building A) and to the existing 300 mm diameter combined sewer in the laneway (Building B) as shown on Figure 6.

Using the Manning formula with an 'n' of 0.013 and a slope of 2.0%, a 200 mm diameter storm connection can convey a flow of 48.4 L/s, while a 100 mm diameter storm connection can convey a flow of 7.6 L/s, conveyances which are sufficient to meet the allowable respective release rates of 35.2 L/s and 4.4 L/s for Buildings A and B. A 100 mm orifice tube will be placed upstream of the control manhole located at Building A to regulate the flow below the allowable maximum discharge rate. For Building B, a 3-inch (76 mm) diameter SXH Hydrobrake valve has been selected to control runoff from the cistern before entering the control manhole.

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## 4.3 WATER BALANCE

The City of Toronto has recently implemented the Wet Weather Flow Guidelines which require a water balance approach to storm runoff and have set as a minimum standard for the retention of all flows from a 5mm storm event utilizing infiltration, evaporation and rainwater reuse. In order to meet the water balance requirements, the developer is proposing to construct cisterns on the P1 level parking garage for Building A and concourse level for Building B. Stormwater collected in the sumps can be reused for irrigation, car washing, or toilet flushing of commercial spaces. Refer to the Stormwater Management Report for further details.

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## 4.4 STORMWATER QUANTITY CONTROLS

### 4.4.1 ALLOWABLE OUTFLOW

The 2-year pre-development peak flow was calculated using the rational method with an inlet time of 10 minutes, a site area of 0.323 ha, and a run-off coefficient of 0.5. The allowable release rate from the sites were calculated to be 39.6 L/s. Refer to Stormwater Management Report for more details.

### 4.4.2 REQUIRED STORAGE

As per City requirements, both the minor and major storm events will be controlled to below the 2-year pre-development rate. The development will require cisterns on the below-ground levels to control the storm flow and release stormwater at the maximum allowable rates. In order to achieve the control of the 100-year storm event, the required storage of the cisterns will be 165 m<sup>3</sup> for Building A and 16 m<sup>3</sup> for Building B.

The modified rational method was used to determine the storage required to control the post development flows down to the allowable release rates. Refer to Stormwater Management Report for the calculations.

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## 4.5 STORMWATER QUALITY CONTROLS

The City of Toronto's Wet Weather Flow Management Guidelines (WWMFG) requires that all new developments provide long term removal of 80% of Total Suspended Solids (TSS) on an average annual basis.

The proposed roof areas for the development will not be prone to sediment generation and can therefore be considered clean for the purposes of storm water quality control. Building A is covered by mostly roof, with some at-grade hardscape and landscaping (POPS), so there will be some at-grade sediment-generating surfaces or activities. Building B is covered mostly by roof. Please refer to the Stormwater Management Report for more details.

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## 4.6 PROPOSED STORM SERVICE - MINOR DRAINAGE SYSTEM

As previously mentioned and in coordination with the Stormwater Management Report, Building A will be serviced by a 200 mm diameter PVC storm connection connecting to the existing 600 mm diameter combined sewer on Yorkville Avenue. Building B will be serviced by a 100 mm diameter PVC storm connection connecting to the existing 300 mm diameter combined sewer in the laneway north of the building. Flow controls will restrict the outflows from both cisterns to the allowable levels.

Installation of these connections will be coordinated with the City of Toronto connections department. All other internal plumbing will meet O.B.C. standards.

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## 4.7 PROPOSED STORM SERVICE - MAJOR STORM DRAINAGE SYSTEM

The major storm drainage will be stored on site and released to the minor storm system at a maximum rate of 39.6 L/s for the site, as indicated in Section 4.4.1 Allowable Outflow. The cisterns will accommodate both the water retention and quantity control, and are currently sized to accommodate 181 m<sup>3</sup> of total storage. The flow controls will control the flow to below the maximum allowable release rate, allowing the storm water to drain by gravity to the control manholes, then to the municipal sewers.

Discharge from the new roof drainage systems and stormwater runoff from the various impervious roof/outdoor amenity and terrace surfaces of the buildings will be directed to the cisterns below ground. The area drains and trench drains will be sized to convey the 100-year storm event to the cisterns without any overflow for all storm events up to the 100-year storm event. The area drains and trench drains will connect through the garage slab to the mechanical storm drainage system inside the buildings which will direct all flows to the cisterns. The building structures will be designed to support the storm water cisterns under the most critical loading conditions (i.e. when cistern is full).

For storms larger than the 100-year design storm, or if the cisterns outlets becomes blocked, the excess water in the cistern will be directed via an overflow hatch onto the grade and drained via the overland flow route to the municipal R.O.W.

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## 4.8 ANALYSIS OF DOWNSTREAM STORM SEWERS

The City of Toronto has provided copies of the City's Dorsch model data and Sewer Atlas Maps for the combined sewers on Yorkville Avenue and in the laneway. Copies of the Dorsch Model and Sewer Atlas Maps are provided in Appendix C and are only used as a reference to complete the design sheet for pre and post development.

As mentioned in Section 2.6 above, storm flows decreased from pre- to post-development as a result of the proposed development. The total pre-development storm flow from the site was calculated to be approximately 72.5 L/s and the total post-development storm flow was calculated to be 31.7 L/s, which results in a net reduction of 40.6 L/s.

Since the proposed site is reducing storm flows contributing to the combined sewer system compared to existing conditions, no downstream wet-weather flow analysis is necessary for the development.

Since the theoretical flows from the proposed development do not negatively impact the existing storm sewer system as demonstrated in the post-development design sheets, WSP has concluded that the downstream sewer system is adequate for the proposed redevelopment and no downstream sewer improvements are required to service this development.







# 5 CONCLUSIONS

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## 5.1 SANITARY

The existing 600 and 675 mm diameter combined sewer on Yorkville Avenue and the existing 300 mm diameter combined sewer in the laneway north of Building B both have sufficient capacity to convey the projected peak sanitary flows. Building A will discharge to the existing 675 mm combined sewer along Yorkville Avenue through one 200 mm diameter residential sanitary service connection and one 100 mm diameter commercial sanitary connection. Building B will discharge flow to the existing 300 mm combined sewer in the laneway north of the building via a 100 mm diameter sanitary service connection. Sanitary control maintenance holes will be installed immediately inside the property lines and will be fitted with backflow prevention devices. The control manholes will be accessible from the outside per City standards. The building sanitary systems will be designed to operate under municipal sewer surcharge conditions.

The downstream combined sewers can adequately accommodate the proposed redevelopment. No downstream combined sewer improvements are required to service the proposed development.

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## 5.2 WATER

Building A will be serviced by two 200 mm diameter PVC fire connections into the existing 300 mm watermain on Yorkville Avenue. Each fire connection will have one 150 mm domestic branch. Building B will be serviced by one shared 150 mm diameter connection, which will connect to the existing 150 mm watermain on Cumberland Street. A water meter and a detector check valve will be installed as close to the property line as possible within both buildings. All internal plumbing will meet Ontario Building Code standards. The two fire connections will be separated by a proposed valve, as required. Once hydrant flow testing has been completed in the spring, the results will be compared with the calculated maximum day plus fire demands from the proposed development.

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## 5.3 STORM

Building A will be serviced by a 200 mm diameter PVC storm connection along the north side of the building and connect into the existing 600 mm combined sewer. Building B will be serviced by a 100 mm diameter PVC storm connection along the north side of the building connecting to the existing 300 mm diameter combined sewer in the laneway. Storm control maintenance holes will be installed immediately inside the property lines. The control manholes will be accessible from the outside per City standard. The building storm systems will be designed to operate under municipal sewer surcharge conditions.

The proposed development will reduce the storm flows coming from the site to the existing combined sewer system to a 2-year pre-development release rate during all storms up to, and including, the 100-year event. Therefore, WSP has concluded that there will be no negative impacts to the existing combined sewer system as a result of this development.

# APPENDIX

# A

## THEORETICAL SANITARY SEWAGE FLOWS & SANITARY DESIGN SHEETS & SANITARY DRAINAGE AREA PLAN (SDR-1)

## APPENDIX A THEORETICAL SANITARY SEWAGE FLOWS

Project: 11 Yorkville Avenue  
Job No.: 17M-01494  
Date: March 27, 2018

### A. Existing Development

Address	Gross Floor Area (GFA) <sup>1</sup>	Site Area	Population <sup>2</sup>	Average Commercial Flow (250 L/cap/d)	Infiltration Allowance (0.26 L/s/ha)	Total Existing Sanitary Flow
	(m <sup>2</sup> )	(ha)	(ppl)	(L/s)	(L/s)	(L/s)
11 Yorkville Avenue	7700	0.077	85	0.25	0.02	0.27
17 Yorkville Avenue	1158	0.039	13	0.04	0.01	0.05
19 Yorkville Avenue	1004	0.025	12	0.03	0.01	0.04
21 Yorkville Avenue	3140	0.079	35	0.10	0.02	0.12
16 Cumberland Street	828	0.021	10	0.03	0.01	0.03
18 Cumberland Street	477	0.016	6	0.02	0.00	0.02
<b>Total</b>	<b>14,307</b>	<b>0</b>	<b>161</b>	<b>0.47</b>	<b>0.07</b>	<b>0.53</b>

Note 1: Approximate GFA for existing commercial buildings

### B. Proposed Development

Residential Unit Type	Total Residential Units	Persons per Unit	Total Residential Population
<b>Building A</b>			
1B, 1B+D & Studio Units	426	1.4	597
2B Units	218	2.1	458
3B Units	72	3.1	224
<b>Total Residential</b>	<b>716</b>	<b>-</b>	<b>1,279</b>
			72.5
			-31.9
Commercial Type	GFA (m <sup>2</sup> )	Density (ppl/100m <sup>2</sup> )	Total Commercial Population
Retail	3,818	1.1	42
			40.6
<b>Building B</b>			
Retail	845.88	1.1	10
<b>Total Commercial</b>	<b>4,664</b>	<b>-</b>	<b>52</b>

### Proposed Flow

Unit Type	Gross Floor Area (m <sup>2</sup> )	Site Area (ha)	Residential Population <sup>1</sup>	Average Residential Flow (450 L/cap/d)		Harmon Peaking Factor	Peak Residential Flow (L/s)	Permanent Dewatering Rate (L/s)	Total Commercial Sanitary Flow (250 L/cap/day) (L/s)	Infiltration Allowance (0.26 L/s/ha) (L/s)	Total Peak Flow <sup>(2)</sup> (L/s)
				(L/s)	(m <sup>3</sup> /day)						
Residential	49,001	0.323	1279	6.661	575.6	3.729	24.84	2.37	0.15	0.08	27.44
			<b>Total Average Flow</b>	<b>6.66</b>	<b>575.55</b>						

Total Peak Flow = 27.44 L/s  
Increase in Peak Flow = 26.91 L/s

Note 1: 1.4 people per 1B & 1B+D & Studio Unit, 2.1 people per 2B Unit, and 3.1 people per 3B Unit per City of Toronto Design Criteria for Sewers and Watermain, November 2009, page 35

Note 2: Commercial Flow rate based on proposed populations and 1.1 persons/100m<sup>2</sup> per City of Toronto Design Criteria for Sewers and Watermain, November 2009, page 34

Peaking Factor = Harmon Formula

### Average Daily Flow

Residential flow is based on 450 L/cap/d, per City of Toronto Design Criteria for Sewers and Watermain, November 2009, page 37

## ZONE/PIPES AREAS

Drainage Zone	Land Use (hectares)				Population		
	Total	Residential	Commercial	Institutional	Residential	Commercial	Institutional
Zone 1	0.510508	0.120457	0.201715	0.188336	49	23	17
Zone 2	0.435289	0.09281	0	0.342479	38	0	30
Zone 3	0.503855	0.133519	0.062196	0.30814	54	7	27
Zone 4	2.875343	1.377012	0.183792	1.314539	551	21	114
Zone 5	1.607135	1.41228	0.029974	0.164881	565	4	15
Zone 6	0.612568	0.348386	0.264182	0	140	30	0
Zone 7	9.829049	7.491855	1.08288	1.254314	2997	120	108
Zone 8	6.390357	5.851752	0.538605	0	2341	60	0
Total	22.764104	16.828071	2.363344	3.572689	6735	265	311

EQUIVALENT POPULATION DENSITIES BASED ON LAND USE:	
RESIDENTIAL	400 persons/ha
INDUSTRIAL	136 persons/ha
OFFICES	330 persons/ha
COMMERCIAL & RETAIL	110 persons/ha
SCHOOLS & CHURCHES	86 persons/ha
HOTELS	400 persons/ha
APARTMENTS	400 persons/ha

Pipe Number	Land Use (hectares)			Length
	Residential	Commercial	Institutional	
11 Yorkville Location Part A	0.162733	0	0	179.34
4355	0.350873	0	0.188336	
11 Yorkville Location Part B	0.162137	0	0	200.84
4356	0.162137	0.117831	0	
16/18 Cumberland	0	0.035629	0	
4357	0.459412	0	0	
4358	0.01417	0	0	
4360	0.038128	0.005599	0.015256	
4361	0.103988	0.026128	0	
4368	0	0	0	
4369	0.107153	0.285402	0	
4370	0.172994	0.10889	0	
4371	0.042091	0.042056	0	
4388	0.172365	0.148568	0	
4389	0.136272	0.173877	0	



**D./ PRE-DEVELOPMENT CONDITIONS - DRY WEATHER**

**Sanitary Flows**  
 Proposed Residential Avg.Daily Flow = 450 L/d  
 Existing Residential Avg.Daily Flow = 240 L/d  
 Existing Commercial Avg.Daily Flow = 250 L/d  
 n= 0.013

**Extraneous Flows**  
 Infiltration Allowance = 0.260 L/s/ha

Design Sheet No **1 of 2**  
 Project: **11 Yorkville**  
 Project no.: **17M-01494**

**COMBINED SEWERSHED AREA: 22.764 ha**

SANITARY FLOW CALCULATIONS      STM SEWER FLOW      BASED ON CITY OF TORONTO ARCHIVE

Description / Location / Dissemination Blocks	PIPE ID	Segment			Cumulative			SANITARY FLOW							STM Flow DQ 2 YEAR (L/s)	Accm STM (L/s)	TOTAL COMBINED FLOW (L/s)	LENGTH (m)	ACTUAL PIPE SIZE (mm)	PIPE AREA (AF) (m2)	SLOPE (%)	CAPACITY (L/s)	VELOCITY (m/s)	TIME OF FLOW (min)	% Full
		Area A (ha)	Population			Area A (ha)	Population			PEAKING FACTOR (M)	Res (L/s)	Emp (L/s)	Infiltration Allowance (L/s)	Acc SAN Flow (L/s)											
			Res	ICI	Total		Res	ICI	Total																
Yonge Street	4369	0.393	43	31	75	18.573	5,018	585	5,607	3.244	45.214	1.691	0.102	47.01		47.01	50.9	900	0.636	1.41	2149.63	3.38	0.25	2.2%	
Yonge Street	4370	0.282	69	12	82	18.855	5,087	597	5,689	3.238	45.759	1.726	0.073	47.56		47.56	40.2	900	0.636	1.14	1932.88	3.04	0.22	2.5%	
Yonge Street	4371	0.084	17	5	22	18.939	5,104	601	5,711	3.237	45.892	1.739	0.022	47.65		47.65	9.4	900	0.636	1.22	1999.55	3.14	0.05	2.4%	
<a href="#">Zone 8 from north along Yonge (4387)</a>		6.390	2,341	60	2,401	25.329	7,445	661	8,112	3.081	63.713	1.913	1.661	67.29		67.29									
Easement	4388	0.321	69	16	86	25.650	7,514	678	8,198	3.077	64.221	1.960	0.083	66.27		66.27	55.8	1500	1.767	3.70	13597.24	7.69	0.12	0.5%	
Easement	4389	0.310	55	19	74	25.961	7,569	697	8,272	3.074	64.623	2.016	0.081	66.72		66.72	67.1	1500	1.767	0.95	6889.88	3.90	0.29	1.0%	
To Rosedale Valley Combined Sewer Trunk														502.38		502.38									

Notes: \* Residential and employment populations derived from site areas and population densities as outlined in City of Toronto Design Criteria for Sewers and Watermains  
 \* Sewer information based on City of Toronto archive drawings  
 \* See Figure 7 for combined sewer tributary areas





**APPENDIX A  
EXISTING COMBINED SEWER ANALYSIS  
POST-DEVELOPMENT DRY WEATHER  
CITY OF TORONTO**

TABLE D.2.1

**D./ POST-DEVELOPMENT CONDITIONS - DRY WEATHER**

Sanitary Flows  
Proposed Residential Avg.Daily Flow = 450 L/d n= 0.013  
Existing Residential Avg.Daily Flow = 240 L/d  
Existing Commercial Avg.Daily Flow = 250 L/d

Extraneous Flows  
Infiltration Allowance = 0.260 L/s/ha

Design Sheet No **2 of 2**  
Project: **11 Yorkville**  
Project no.: **17M-01494**

**COMBINED SEWERSHED AREA: 22.764 ha**

Description / Location / Dissemination Blocks	PIPE ID	SANITARY FLOW CALCULATIONS													STM SEWER FLOW		BASED ON CITY OF TORONTO ARCHIVE							
		Segment			Cumulative			SANITARY FLOW					STM Flow DQ 2 YEAR (L/s)	Accm STM (L/s)	TOTAL COMBINED FLOW (L/s)	LENGTH (m)	ACTUAL PIPE SIZE (mm)	PIPE AREA (AF) (m2)	SLOPE (%)	CAPACITY (L/s)	VELOCITY (m/s)	TIME OF FLOW (min)	% Full	
		Area A (ha)	Population		Area A (ha)	Population		PEAKING FACTOR	Res	Emp	Infiltration Allowance1	Acc SAN Flow												
Res	ICI	Total	Res	ICI	Total	M	(L/s)	(L/s)	(L/s)	(L/s)														
Yonge Street	4369	0.393	43	31	75	16.952	4,634	521	6,807	3.275	42.163	1.507	0.102	<b>43.77</b>		<b>43.77</b>	50.9	900	0.636	1.41	<b>2149.63</b>	3.38	0.25	2.0%
Yonge Street	4370	0.282	69	12	82	17.234	4,703	533	6,889	3.270	42.716	1.542	0.073	<b>44.33</b>		<b>44.33</b>	40.2	900	0.636	1.14	<b>1932.88</b>	3.04	0.22	2.3%
Yonge Street	4371	0.084	17	5	22	17.319	4,720	537	6,911	3.268	42.850	1.555	0.022	<b>44.43</b>		<b>44.43</b>	9.4	900	0.636	1.22	<b>1999.55</b>	3.14	0.05	2.2%
<b>Zone 8 from north along Yonge (4387)</b>		<b>6.390</b>	<b>2,341</b>	<b>60</b>	<b>2,401</b>	<b>23.709</b>	<b>7,061</b>	<b>597</b>	<b>9,312</b>	<b>3.103</b>	<b>60.863</b>	<b>1.729</b>	<b>1.661</b>	<b>64.25</b>		<b>64.25</b>								
Easement	4388	0.321	69	16	86	24.030	7,130	614	9,398	3.099	61.376	1.776	0.083	<b>63.24</b>		<b>63.24</b>	55.8	1500	1.767	3.70	<b>13597.24</b>	7.69	0.12	0.5%
Easement	4389	0.310	55	19	74	24.340	7,185	633	9,472	3.096	61.781	1.831	0.081	<b>63.69</b>		<b>63.69</b>	67.1	1500	1.767	0.95	<b>6889.88</b>	3.90	0.29	0.9%
To Rosedale Valley Combined Sewer Trunk														<b>466.43</b>		<b>466.43</b>								

Notes: \* Residential and employment populations derived from site areas and population densities as outlined in City of Toronto Design Criteria for Sewers and Watermains  
\* Sewer information based on City of Toronto archive drawings  
\* See Figure 8 for combined sewer tributary areas

## APPENDIX A

TABLE D.1.2

A./ PRE-DEVELOPMENT CONDITIONS - 2-yr WET WEATHER		<div style="display: flex; justify-content: space-between;"> <div style="width: 30%;"> <p><b>Sanitary Flows</b></p> <p>Proposed Residential Avg. Daily Flow = 450 L/d                      Existing Residential Avg. Daily Flow = 240 L/d                      Existing Commercial Avg. Daily Flow = 250 L/d</p> <p><b>Extraneous Flows</b></p> <p>Infiltration Allowance = 0.260 L/s/ha                      Foundation Drainage Allowance = 3.0 L/s/ha (ss than 10 ha)</p> </div> <div style="width: 30%;"> <p>Manning's n= 0.013                      C = 0.5</p> <p style="text-align: center;"><b>2 YEAR</b></p> <p>a= 21.800                      b= -0.780                      I= 88.19</p> </div> <div style="width: 30%; text-align: right;"> <p>Design Sheet No 1 of 6                      Project: 11 Yorkville                      Project no.: 17M-01494</p> </div> </div>																															
		COMBINED SEWERSHED AREA: 22.764 ha																															
SANITARY FLOW CALCULATIONS										STM SEWER FLOW										BASED ON CITY OF TORONTO ARCHIVE													
Description / Location / Dissemination Blocks	PIPE ID	Segment			Cumulative			SANITARY FLOW						STORM TRIBUTARY AREA (ha)	RUNOFF COEF. C	A X C	ACCUM. A X C	Tc (min.)	INTENSITY (mm/hr)	Accm STM (L/s)	TOTAL COMBINED FLOW (L/s)	LENGTH (m)	ACTUAL PIPE SIZE (mm)	PIPE AREA (AF) (m2)	SLOPE (%)	CAPACITY (L/s)	VELOCITY (m/s)	TIME OF FLOW (min)	% Full				
		Area A (ha)	Population		Area A (ha)	Population		PEAKING FACTOR M	Res (L/s)	Emp (L/s)	Infiltration Allowance (L/s)	Foundation Drainage (L/s)	Acc SAN Flow (L/s)																				
			Res	ICI		Total	Res																							ICI	Total		
Zone 1 from west along Yorkville (4354)		0.511	49	40	89	0.511	49	40	89	4.000	0.544	0.116	0.133	1.532	2.32	0.51	0.90	0.46	0.46	10.0	88.189	116.3	118.61	134.8							1.50	1.50	
11 Yorkville Location Part A		0.163	65	0	66	0.673	114	40	155	4.000	1.268	0.116	0.042	0.488	1.91	0.16	0.90	0.15	0.61	12.0	76.535	133.1	135.01	179.3							1.50	1.99	
Yorkville Avenue	4355	0.539	140	21	162	1.050	189	61	251	4.000	2.104	0.176	0.140	1.618	4.04	0.54	0.90	0.49	1.09	12.8	72.608	227.4	231.43	66.4	600	0.283	0.37	373.49	1.32	0.84	62.0%		
11 Yorkville Location Part B		0.162	65	0	65	1.212	254	61	316	4.000	2.824	0.176	0.042	0.486	3.53	0.16	0.90	0.15	1.24	15.1	64.072	227.5	231.02	200.8							1.50	2.23	
Yorkville Avenue	4356	0.280	65	13	78	1.330	254	74	329	4.000	2.824	0.213	0.073	0.840	3.95	0.28	0.90	0.25	1.49	15.3	63.282	270.5	274.40	20.4	675	0.358	0.36	504.35	1.41	0.24	54.4%		
Yorkville Avenue	4357	0.459	184	0	184	1.789	438	74	513	4.000	4.866	0.213	0.119	1.378	6.58	0.46	0.90	0.41	1.90	15.7	61.882	337.9	344.48	42.1	675	0.358	0.45	563.88	1.58	0.45	61.1%		
Yorkville Avenue	4358	0.014	6	0	6	1.803	444	74	519	4.000	4.929	0.213	0.004	0.043	5.19	0.01	0.90	0.01	1.92	15.9	61.400	337.5	342.70	15.5	600	0.283	0.56	459.48	1.63	0.16	74.6%		
Zone 2 from south along Yonge (4359)		0.435	38	30	68	2.239	482	104	587	3.983	5.328	0.300	0.113	1.306	7.05	0.44	0.90	0.39	2.31	18.8	53.857	356.6	363.65	262.0							1.50	2.91	
Yonge Street	4360	0.059	15	1	16	2.298	497	104	603	3.976	5.487	0.302	0.015	0.177	5.98	0.06	0.90	0.05	2.36	19.2	53.077	359.5	365.51	27.4	675	0.358	0.30	460.41	1.29	0.35	79.4%		
Zone 3 from east along Collier (5569)		0.504	54	34	88	2.801	551	138	691	3.952	6.048	0.400	0.131	1.512	8.09	0.50	0.90	0.45	2.81	22.4	46.996	379.5	387.59	291.3							1.50	3.24	
Yonge Street	4361	0.130	42	3	45	2.932	592	141	736	3.935	6.476	0.408	0.034	0.390	7.31	0.13	0.90	0.12	2.93	22.9	46.177	388.4	395.71	55.2	750	0.442	0.51	795.04	1.80	0.51	49.8%		
Zone 5 from west along Scollard (4367)		1.607	565	19	584	4.539	1,157	160	1,320	3.758	12.083	0.463	0.418	4.821	17.79	1.61	0.90	1.45	4.38	28.1	39.430	495.3	513.12	463.1							1.50	5.15	
Zone 4 from west along Scollard (4367)		2.875	551	135	686	7.414	1,708	295	2,006	3.638	17.265	0.854	0.748	8.626	27.49	2.88	0.60	1.73	6.10	33.2	34.579	605.6	633.10	463.1							1.50	5.15	
Yonge Street	4368	0.000	0	0	0	7.414	1,708	295	2,006	3.638	17.265	0.854	0.000	0.000	18.12	0.00	0.90	0.00	6.10	33.3	34.505	604.3	622.44	28.0	750	0.442	4.17	2273.38	5.15	0.09	27.4%		
Zone 6 from east along Church (5539) and Zone 7 from west along Davenport (4352)		10.442	3,137	258	3,395	17.856	4,845	553	5,401	3.258	43.846	1.601	2.715	31.325	79.49	10.44	0.90	9.40	15.50	40.7	29.496	1312.1	1391.60	667.6							1.50	7.42	
Yonge Street	4369	0.393	43	31	75	18.248	4,888	585	5,476	3.254	44.186	1.691	0.102	1.178	47.16	0.39	0.90	0.35	15.85	41.0	29.355	1335.6	1382.76	50.9	900	0.636	1.41	2149.63	3.38	0.25	64.3%		
Yonge Street	4370	0.282	69	12	82	18.530	4,958	597	5,558	3.248	44.734	1.726	0.073	0.846	47.38	0.28	0.90	0.25	16.11	41.2	29.232	1351.3	1398.68	40.2	900	0.636	1.14	1932.88	3.04	0.22	72.4%		
Yonge Street	4371	0.084	17	5	22	18.614	4,974	601	5,580	3.247	44.867	1.739	0.022	0.252	46.88	0.08	0.90	0.08	16.18	41.2	29.205	1356.4	1403.26	9.4	900	0.636	1.22	1999.55	3.14	0.05	70.2%		
Zone 8 from north along Yonge (4387)		6.390	2,341	60	2,401	25.005	7,315	661	7,981	3.088	62.751	1.913	1.661	19.171	85.50	6.39	0.90	5.75	21.93	49.9	25.190	1585.7	1671.19	774.9							1.50	8.61	
Easement	4388	0.321	69	16	86	25.325	7,384	678	8,067	3.084	63.262	1.960	0.083	0.963	66.27	0.32	0.90	0.29	22.22	50.0	25.142	1603.5	1669.81	55.8	1500	1.767	3.70	13597.24	7.69	0.12	12.3%		
Easement	4389	0.310	55	19	74	25.636	7,439	697	8,141	3.081	63.665	2.016	0.081	0.930	66.69	0.31	0.90	0.28	22.50	50.3	25.030	1616.4	1683.14	67.1	1500	1.767	0.95	6889.88	3.90	0.29	24.4%		
To Rosedale Valley Combined Sewer Trunk															558.71							15000.5	15559.19										

Notes: \* Residential and employment populations derived from site areas and population densities as outlined in City of Toronto Design Criteria for Sewers and Watermains  
 \* Sewer information based on City of Toronto archive drawings  
 \* See Figure SAN-1 for combined sewer tributary areas

# APPENDIX A

TABLE D.2.2

## A./ POST-DEVELOPMENT CONDITIONS - 2-yr WET WEATHER

**Sanitary Flows**  
 Proposed Residential Avg.Daily Flow = 450 L/d  
 Existing Residential Avg.Daily Flow = 240 L/d  
 Existing Commercial Avg.Daily Flow = 250 L/d

**Extraneous Flows**  
 Infiltration Allowance = 0.260 L/s/ha  
 Foundation Drainage Allowance = 3.0 L/s/ha ss than 10 ha)

Manning's n= 0.013  
 C = 0.5  
**2 YEAR**  
 a= 21.800  
 b= -0.780  
 I= 88.19

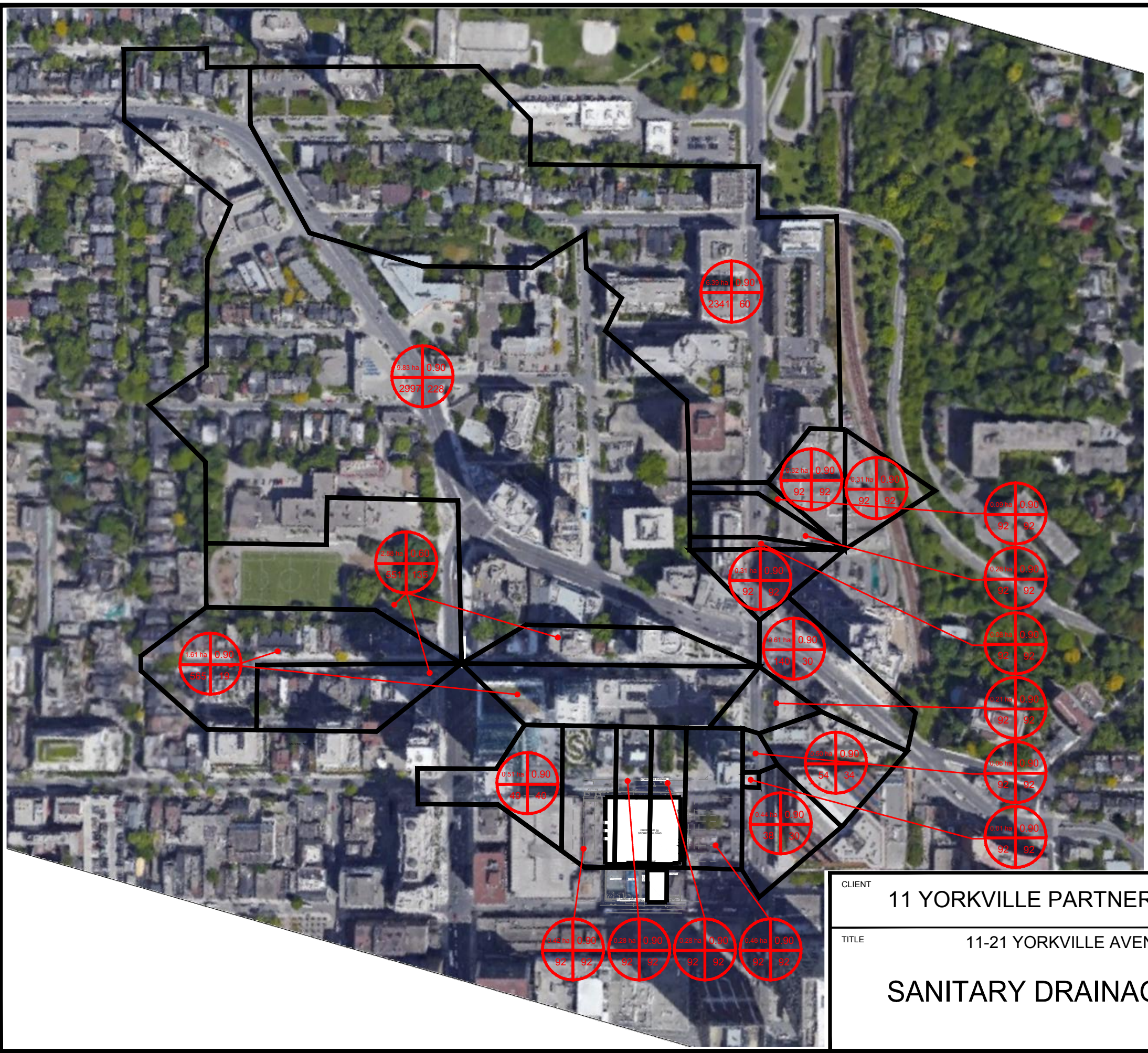
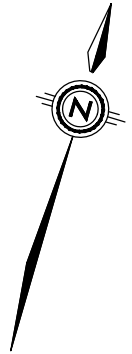
Design Sheet No 1 of 6  
 Project: 11 Yorkville  
 Project no.: 17M-01494

**COMBINED SEWERSHED AREA: 22.764 ha**






Description / Location / Dissemination Blocks	PIPE ID	SANITARY FLOW CALCULATIONS														STM SEWER FLOW						BASED ON CITY OF TORONTO ARCHIVE											
		Segment			Cumulative			SANITARY FLOW								STORM TRIBUTARY AREA (ha)	RUNOFF COEF. C	A X C	ACCUM. A X C	Tc (min.)	INTENSITY (mm/hr)	Accm STM (L/s)	TOTAL COMBINED FLOW (L/s)	LENGTH (m)	ACTUAL PIPE SIZE (mm)	PIPE AREA (AF) (m2)	SLOPE (%)	CAPACITY (L/s)	VELOCITY (m/s)	TIME OF FLOW (min)	% Full		
		Area A (ha)	Population		Area A (ha)	Population		PEAKING FACTOR M	Res (L/s)	Emp (L/s)	Infiltration Allowance (L/s)	Foundation Drainage (L/s)	Acc SAN Flow (L/s)																				
			Res	ICI		Total	Res							ICI	Total																		
Zone 1 from west along Yorkville (4354)		0.511	49	40	89	0.511	49	40	89	4.000	0.544	0.116	0.133	1.532	2.32	0.51	0.90	0.46	0.46	10.0	88.189	116.3	118.61	134.8							1.50	1.50	
Yorkville Avenue	4355	0.539	140	21	162	1.050	189	61	251	4.000	2.104	0.176	0.140	1.618	4.04	0.54	0.90	0.49	0.94	10.8	82.825	224.6	228.61	66.4	600	0.283	0.37	373.49	1.32	0.84	61.2%		
11 Yorkville		0.323	1,096	43	1,139	1.373	1,285	104	1,390	3.727	13.307	0.300	0.084	2.269	15.96	0.32	0.90	0.29	1.24	13.1	71.571	253.8	269.73	200.8							1.50	2.23	
Yorkville Avenue	4356	0.280	65	13	78	1.330	254	74	329	4.000	2.824	0.213	0.073	0.840	3.95	0.28	0.90	0.25	1.49	13.3	70.557	301.2	305.15	20.4	675	0.358	0.36	504.35	1.41	0.24	60.5%		
16/18 Cumberland Street		0.034	0	10	10	0.034	0	10	10	4.000	0.000	0.029	0.009	0.10	0.14	0.03	0.90	0.03	0.03	10.0	88.189	7.7	7.89										
Yorkville Avenue	4357	0.459	184	0	184	1.789	438	74	513	4.000	4.866	0.213	0.119	1.378	6.58	0.46	0.90	0.41	1.90	13.8	68.769	375.2	381.75	42.1	675	0.358	0.45	563.88	1.58	0.45	67.7%		
Yorkville Avenue	4358	0.014	6	0	6	1.803	444	74	519	4.000	4.929	0.213	0.004	0.043	5.19	0.01	0.90	0.01	1.91	13.9	68.156	374.3	379.51	15.5	600	0.283	0.56	459.48	1.63	0.16	82.6%		
Zone 2 from south along Yonge (4359)		0.435	38	30	68	2.239	482	104	587	3.983	5.328	0.300	0.113	1.306	7.05	0.44	0.90	0.39	2.31	16.8	58.770	388.8	395.90	262.0							1.50	2.91	
Yonge Street	4360	0.059	15	1	16	2.298	497	104	603	3.976	5.487	0.302	0.015	0.177	5.98	0.06	0.90	0.05	2.36	17.2	57.820	391.4	397.36	27.4	675	0.358	0.30	460.41	1.29	0.35	86.3%		
Zone 3 from east along Collier (5569)		0.504	54	34	88	2.801	551	138	691	3.952	6.048	0.400	0.131	1.512	8.09	0.50	0.90	0.45	2.81	20.4	50.537	407.8	415.94	291.3							1.50	3.24	
Yonge Street	4361	0.130	42	3	45	2.932	592	141	736	3.935	6.476	0.408	0.034	0.390	7.31	0.13	0.90	0.12	2.93	20.9	49.571	416.7	424.03	55.2	750	0.442	0.51	795.04	1.80	0.51	53.3%		
Zone 5 from west along Scollard (4367)		1.607	565	19	584	4.539	1,157	160	1,320	3.758	12.083	0.463	0.418	4.821	17.79	1.61	0.90	1.45	4.38	26.1	41.761	524.4	542.21	463.1							1.50	5.15	
Zone 4 from west along Scollard (4367)		2.875	551	135	686	7.414	1,708	295	2,006	3.638	17.265	0.854	0.748	8.626	27.49	2.88	0.60	1.73	6.10	31.2	36.288	635.4	662.87	463.1							1.50	5.15	
Yonge Street	4368	0.000	0	0	0	7.414	1,708	295	2,006	3.638	17.265	0.854	0.000	0.000	18.12	0.00	0.90	0.00	6.10	31.3	36.206	633.9	652.06	28.0	750	0.442	4.17	2273.38	5.15	0.09	28.7%		
Zone 6 from east along Church (5539) and Zone 7 from west along Davenport (4352)		10.442	3,137	258	3,395	17.856	4,845	553	5,401	3.258	43.846	1.601	2.715	31.325	79.49	10.44	0.90	9.40	15.50	38.7	30.673	1364.3	1443.82	667.6							1.50	7.42	
Yonge Street	4369	0.393	43	31	75	18.248	4,888	585	5,476	3.254	44.186	1.691	0.102	1.178	47.16	0.39	0.90	0.35	15.85	39.0	30.519	1388.4	1435.57	50.9	900	0.636	1.41	2149.63	3.38	0.25	66.8%		
Yonge Street	4370	0.282	69	12	82	18.530	4,958	597	5,558	3.248	44.734	1.726	0.073	0.846	47.38	0.28	0.90	0.25	16.11	39.2	30.385	1404.4	1451.82	40.2	900	0.636	1.14	1932.88	3.04	0.22	75.1%		
Yonge Street	4371	0.084	17	5	22	18.614	4,974	601	5,580	3.247	44.867	1.739	0.022	0.252	46.88	0.08	0.90	0.08	16.18	39.2	30.355	1409.6	1456.53	9.4	900	0.636	1.22	1999.55	3.14	0.05	72.8%		
Zone 8 from north along Yonge (4387)		6.390	2,341	60	2,401	25.005	7,315	661	7,981	3.088	62.751	1.913	1.661	19.171	85.50	6.39	0.90	5.75	21.93	47.9	26.004	1636.8	1722.32	774.9							1.50	8.61	
Easement	4388	0.321	69	16	86	25.325	7,384	678	8,067	3.084	63.262	1.960	0.083	0.963	66.27	0.32	0.90	0.29	22.22	48.0	25.953	1655.1	1721.39	55.8	1500	1.767	3.70	13597.24	7.69	0.12	12.7%		
Easement	4389	0.310	55	19	74	25.636	7,439	697	8,141	3.081	63.665	2.016	0.081	0.930	66.69	0.31	0.90	0.28	22.50	48.3	25.832	1668.1	1734.83	67.1	1500	1.767	0.95	6889.88	3.90	0.29	25.2%		
To Rosedale Valley Combined Sewer Trunk															569.37							15578.5	16147.89										

Notes: \* Residential and employment populations derived from site areas and population densities as outlined in City of Toronto Design Criteria for Sewers and Watermains  
 \* Sewer information based on City of Toronto archive drawings  
 \* See Figure SAN-1 for combined sewer tributary areas






**LEGEND**

-  AREA
-  DRAINAGE COEFFICIENT
-  ICI POPULATION
-  RESIDENTIAL POPULATION
-  LIMIT OF PROP. WORKS

PLOTDATE: Mar 27, 2018 - 11:01am. israc.alexander-cook

CLIENT	11 YORKVILLE PARTNERSHIP INC.	
TITLE	11-21 YORKVILLE AVENUE	
	<b>SANITARY DRAINAGE PLAN</b>	

			
Checked	B.S.T.	Drawn	10/12 Cad
Date	MAR. 2018	Proj. No.	17M-01494
Scale	NTS	Figure No.	SAN-1



## APPENDIX

# B

## DOMESTIC WATER DEMAND, HYDRANT FLOW TESTING RESULTS AND FUS FIRE FLOW CALCULATIONS

## THEORETICAL DOMESTIC WATER DEMAND CALCULATIONS APPENDIX B

Project: 11 Yorkville Avenue  
 Job No.: 17M-01494  
 Date: March 25, 2018

### Proposed Development

Unit Type	Gross Floor Area (m <sup>2</sup> )	Bedrooms # units	Population <sup>1,2</sup>	Average Water Demand <sup>3</sup> (191 L/cap/d)		Peaking Factor <sup>4</sup>		Peak Water Demand	
				(L/s)	(m <sup>3</sup> /day)	Peak Hour	Max. Day	Peak Hour (L/s)	Max. Day (L/s)
1 Bedroom Unit		426	597	1.32	114.03	2.50	1.30	3.299	1.716
2 Bedroom Unit		218	458	1.01	87.48	2.50	1.30	2.531	1.316
3 Bedroom Unit		72	224	0.50	42.78	2.50	1.30	1.238	0.644
Retail - Building A	3,818	-	42	0.09	8.02	1.20	1.10	0.111	0.102
	<b>Total - Building A</b>	<b>716</b>	<b>1321</b>	<b>2.92</b>	<b>252.31</b>	-	-	<b>7.18</b>	<b>3.78</b>
Retail - Building B	846	-	10	0.02	1.91	1.20	1.10	0.027	0.024
	<b>Total - Building B</b>	<b>-</b>	<b>10</b>	<b>0.02</b>	<b>1.91</b>	-	-	<b>0.03</b>	<b>0.02</b>
	<b>Total - Site</b>	<b>716</b>	<b>1331</b>	<b>2.94</b>	<b>254.22</b>	-	-	<b>7.21</b>	<b>3.81</b>

Note 1: Population equivalent for apartments or condominiums per City of Toronto Design Criteria for Sewers and Watermain:

1 bedroom	1.4 person / unit
2 bedroom	2.1 person / unit
3 bedroom	3.1 person / unit
Townhouse	2.7 person / unit

For 1 bedroom + Den and 2 bedroom + Den, we interpolated.

Note 2: 1.1 people per 100 m<sup>2</sup> of commercial retail space, per City of Toronto Design Criteria for Sewers and Watermain

3.3 people per 100 m<sup>2</sup> of office space, per City of Toronto Design Criteria for Sewers and Watermain

Note 3: Water Demand for Multi-Unit Buildings, per City of Toronto Design Criteria for Sewers and Watermain

Note 4: Peaking Factor for apartments and commercial uses are per City of Toronto Design Criteria for Sewers and Watermain

**APPENDIX B**  
**FIRE FLOW CALCULATIONS**  
**Building A**

**Project:** 11 Yorkville Avenue  
**Job No.:** 17M-01494  
**Date:** March 25, 2018

Fire flow required for a given area based on Fire Underwriters Survey (FUS) Water Supply for Public Fire Protection (1999)

$$F = 220 C \sqrt{A}$$

where

F = Fire flow in Litres per minute (Lpm)  
C = coefficient related to the type of construction  
A = total floor area in square metres

**Calculations per FUS**

1. *Estimate of Fire Flow*  
C = 0.6 for fire resistive construction  
A = 2983.36 m<sup>2</sup>  
  
F = 7,000 Lpm (ROUNDED TO NEAREST 1000L/min)

2. *Occupancy Reduction*  
25% reduction based on low hazard occupancy  
  
25% reduction of 7000 Lpm = 1,750 Lpm  
F = 7000 - 1750 = 5,250 Lpm

3. *Sprinkler Reduction*  
30% reduction for NFPA Sprinkler System<sup>2</sup>  
  
30% reduction of 5250 Lpm = 1,575 Lpm  
F = 5250 - 1575 = 3,675 Lpm

4. *Separation Charge*

Face	Distance (m)	Charge
West Side	20.20	10%
East Side	18.00	15%
North Side	20.50	10%
South Side	6.20	20%
Total		55%

of 5,250 = 2,888 Lpm

F = 3675 + 2888  
F = 6,563 Lpm (2,000 Lpm < F < 45,000 Lpm; OK)  
F = 1,732 US GPM

**Notes**

1. If vertical openings and exterior vertical communications are properly protected, (one hour rating) consider only the area of the largest floor plus 25 % of each of the two immediately adjoining floors.
2. Sprinkler protection.

**APPENDIX B**  
**FIRE FLOW CALCULATIONS**  
**Building B**

**Project:** 11 Yorkville Avenue  
**Job No.:** 17M-01494  
**Date:** March 25, 2018

Fire flow required for a given area based on Fire Underwriters Survey (FUS) Water Supply for Public Fire Protection (1999)

$$F = 220 C \sqrt{A}$$

where

F = Fire flow in Litres per minute (Lpm)  
C = coefficient related to the type of construction  
A = total floor area in square metres

**Calculations per FUS**

1. *Estimate of Fire Flow*  
C = 0.6 for fire resistive construction  
A = 462.99 m<sup>2</sup>  
  
F = 3,000 Lpm (ROUNDED TO NEAREST 1000L/min)

2. *Occupancy Reduction*  
25% reduction based on low hazard occupancy  
  
25% reduction of 3000 Lpm = 750 Lpm  
F = 3000 - 750 = 2,250 Lpm

3. *Sprinkler Reduction*  
30% reduction for NFPA Sprinkler System<sup>2</sup>  
  
30% reduction of 2250 Lpm = 675 Lpm  
F = 2250 - 675 = 1,575 Lpm

4. *Separation Charge*

Face	Distance (m)	Charge
West Side	0.00	25%
East Side	0.00	25%
North Side	6.20	20%
South Side	12.50	15%
Total		85%

of 2,250 = 1,913 Lpm

F = 1575 + 1913  
F = 3,488 Lpm (2,000 Lpm < F < 45,000 Lpm; OK)  
F = 920 US GPM

**Notes**

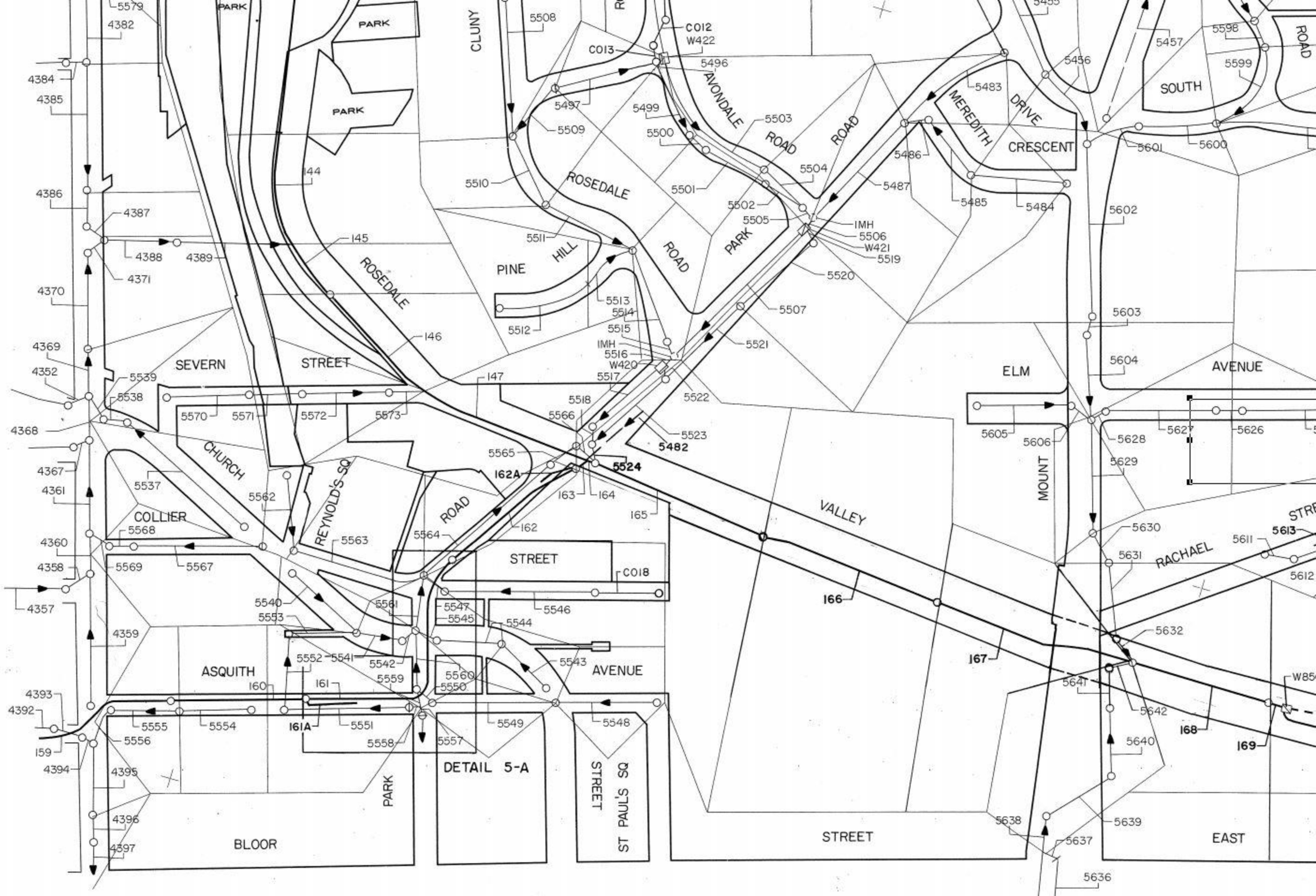
- If vertical openings and exterior vertical communications are properly protected, (one hour rating) consider only the area of the largest floor plus 25 % of each of the two immediately adjoining floors.
- Sprinkler protection.



# APPENDIX

# C

## CITY OF TORONTO DORSCH MODEL SHEETS & SEWER ATLAS MAPS





SOUTH CALCULATION AREA

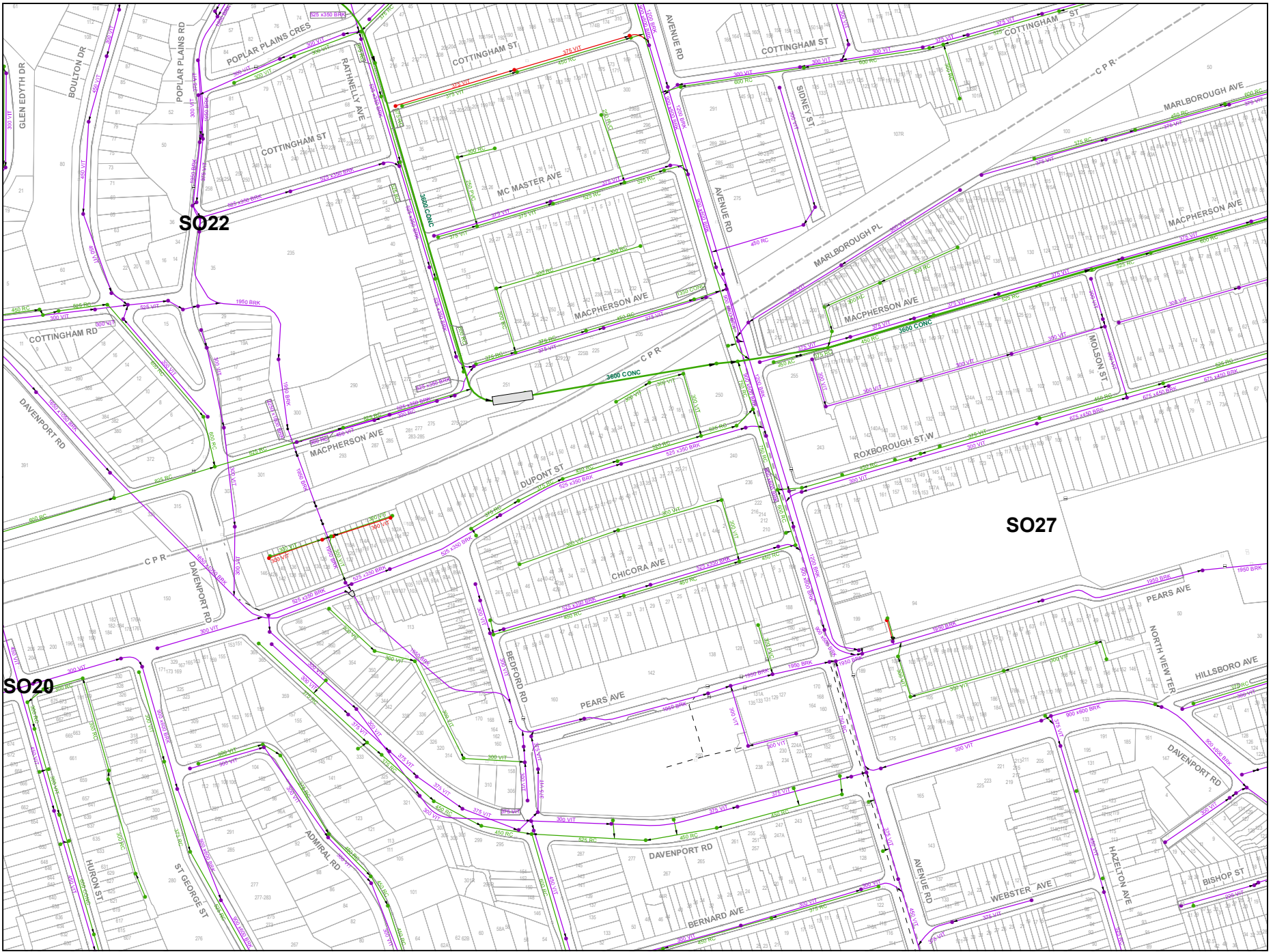
4356	CIRCULAR		0.69/0.69	INFLOW	4355		OUTFLOW	4357		B.NO.	86700		EXIST.	COMB.0004356
	YU 112.238	YL 112.165	QF 532	DQ 0	QDLM 1	VNIGHT0.22	DUC 0.14	DLC 0.18	QLM 366	DUS -2.98	DLS -3.10	RAIN 8MS2	CAP 0000165	QLM/8600069
	SU 116.048	SL 116.142	AF 0.373	DQD 0.0	HDLM 0.02	HNIGHT0.00								
+	RES 44	A 0.0	VF 1.42	GAMMA 0.93	VDLM 0.30	VNORM 0.0	HUM 0.83	HLM 0.87	QRQLM 366	YUM 113.06	YLM 113.04	VLM 1.43	DY 0000007	DH 0000005
	IW 0.0	L 20.4	S 1/ 280	N 0.0130	SCOD 004	DWB 0.0								
4357	CIRCULAR		0.69/0.69	INFLOW	4356		OUTFLOW	4358		B.NO.	86700		EXIST.	COMB.0004357
	YU 112.147	YL 111.958	QF 596	DQ 144	QDLM 1	VNIGHT0.25	DUC 0.20	DLC 0.32	QLM 479	DUS -3.10	DLS -3.18	RAIN 8MS2	CAP 0000117	QLM/8600080
	SU 116.142	SL 116.155	AF 0.373	DQD 0.3	HDLM 0.02	HNIGHT0.00								
+	RES 44	A 0.54	VF 1.60	GAMMA 0.93	VDLM 0.35	VNORM 0.0	HUM 0.89	HLM 1.01	QRQLM 478	YUM 113.04	YLM 112.97	VLM 1.65	DY 0000019	DH 0000012
	IW 0.0	L 42.1	S 1/ 223	N 0.0130	SCOD 004	DWB 0.0								
4358	CIRCULAR		0.69/0.69	INFLOW	4357		OUTFLOW	4360		B.NO.	86700		EXIST.	COMB.0004358
	YU 111.918	YL 111.830	QF 669	DQ 0	QDLM 1	VNIGHT0.28	DUC 0.36	DLC 0.42	QLM 469	DUS -3.18	DLS -3.31	RAIN 8MS2	CAP 0000200	QLM/8600070
	SU 116.155	SL 116.249	AF 0.373	DQD 0.0	HDLM 0.02	HNIGHT0.00								
+	RES 44	A 0.0	VF 1.79	GAMMA 0.93	VDLM 0.38	VNORM 0.0	HUM 1.05	HLM 1.11	QRQLM 468	YUM 112.97	YLM 112.94	VLM 1.35	DY 0000009	DH 0000006
	IW 0.0	L 15.5	S 1/ 177	N 0.0130	SCOD 004	DWB 0.0								
4359	CIRCULAR		0.38/0.38	INFLOW	4359		OUTFLOW	4360		B.NO.	85630		EXIST.	COMB.0004359
	YU 112.707	YL 112.079	QF 160	DQ 130	QDLM 0	VNIGHT0.22	DUC -0.07	DLC 0.51	QLM 111	DUS -3.10	DLS -3.28	RAIN 8MS2	CAP 0000049	QLM/8600069
	SU 116.109	SL 116.249	AF 0.113	DQD 0.2	HDLM 0.01	HNIGHT0.00								
+	RES 32	A 0.45	VF 1.41	GAMMA 1.00	VDLM 0.25	VNORM 0.0	HUM 0.31	HLM 0.89	QRQLM 111	YUM 113.01	YLM 112.97	VLM 1.29	DY 0000063	DH 0000059
	IW 0.0	L 80.5	S 1/ 128	N 0.0130	SCOD 004	DWB 0.0								
4360	CIRCULAR		0.69/0.69	INFLOW	4359	4358	OUTFLOW	4361		B.NO.	85640		EXIST.	COMB.0004360
*	YU 111.772	YL 111.689	QF 489	DQ 0	QDLM 1	VNIGHT0.20	DUC 0.45	DLC 0.45	QLM 568	DUS -3.34	DLS -3.39	RAIN 8MS2	CAP 0000078	QLM/8601016
	SU 116.249	SL 116.219	AF 0.373	DQD 0.0	HDLM 0.02	HNIGHT0.01								
+	RES 32	A 0.0	VF 1.31	GAMMA 1.00	VDLM 0.31	VNORM 0.0	HUM 1.14	HLM 1.14	QRQLM 567	YUM 112.91	YLM 112.83	VLM 1.52	DY 0000008	DH 0000000
	IW 0.0	L 27.4	S 1/ 330	N 0.0130	SCOD 004	DWB 0.0								
4361	CIRCULAR		0.77/0.76	INFLOW	4360	5569	OUTFLOW	4368		B.NO.	85650		EXIST.	COMB.0004361
*	YU 111.625	YL 111.345	QF 819	DQ 83	QDLM 1	VNIGHT0.28	DUC 0.44	DLC 0.60	QLM 635	DUS -3.39	DLS -3.02	RAIN 8MS2	CAP 0000184	QLM/8600078
	SU 116.219	SL 115.725	AF 0.453	DQD 0.1	HDLM 0.02	HNIGHT0.00								
+	RES 32	A 0.29	VF 1.81	GAMMA 1.00	VDLM 0.39	VNORM 0.0	HUM 1.20	HLM 1.36	QRQLM 634	YUM 112.83	YLM 112.70	VLM 1.86	DY 0000028	DH 0000015
	IW 0.0	L 55.2	S 1/ 197	N 0.0130	SCOD 004	DWB 0.0								
4362	CIRCULAR		0.38/0.38	INFLOW	4362		OUTFLOW	4363	P109	B.NO.	69670		EXIST.	COMB.0004362
*	YU 114.207	YL 113.902	QF 112	DQ 169	QDLM 0	VNIGHT0.15	DUC -0.10	DLC 0.03	QLM 162	DUS -1.93	DLS -2.37	RAIN 8MS2	CAP 0000049	QLM/8601045
	SU 116.417	SL 116.682	AF 0.113	DQD 0.5	HDLM 0.02	HNIGHT0.00								
+	RES 53	A 0.81	VF 0.99	GAMMA 0.70	VDLM 0.27	VNORM 0.0	HUM 0.28	HLM 0.41	QRQLM 162	YUM 114.48	YLM 114.32	VLM 1.43	DY 0000031	DH 0000014
	IW 0.0	L 79.3	S 1/ 260	N 0.0130	SCOD 001	DWB 0.0								

Contractions used in HVM output...

1st line: pipe number, cross-section, pipe size...width/height(m), inflow and outflow pipes, block number, sewer type, pipe no.

2nd line: YU, YL = upper and lower invert elevations (m)





**Toronto Sewer Atlas**

- |   |  |  |   |
|---|--|--|---|
| <ul style="list-style-type: none"> <li>Large Chamber</li> <li>Manhole           <ul style="list-style-type: none"> <li>Combined</li> <li>Dual</li> <li>Sanitary</li> <li>Storm</li> <li>Foundation</li> </ul> </li> </ul> | <ul style="list-style-type: none"> <li>Control Manhole           <ul style="list-style-type: none"> <li>Combined</li> <li>Dual</li> <li>Sanitary</li> <li>Storm</li> </ul> </li> </ul> | <ul style="list-style-type: none"> <li>Outfall           <ul style="list-style-type: none"> <li>Outfall</li> <li>Sewer Pump Station</li> <li>Sewer Pump Station</li> <li>Catchbasin               <ul style="list-style-type: none"> <li>Other</li> <li>Twin Inlet Catchbasin</li> </ul> </li> </ul> </li> </ul> | <ul style="list-style-type: none"> <li>Sewer           <ul style="list-style-type: none"> <li>Foundation Drain</li> <li>Combined</li> <li>Sanitary</li> </ul> </li> </ul> |
|---|--|--|---|

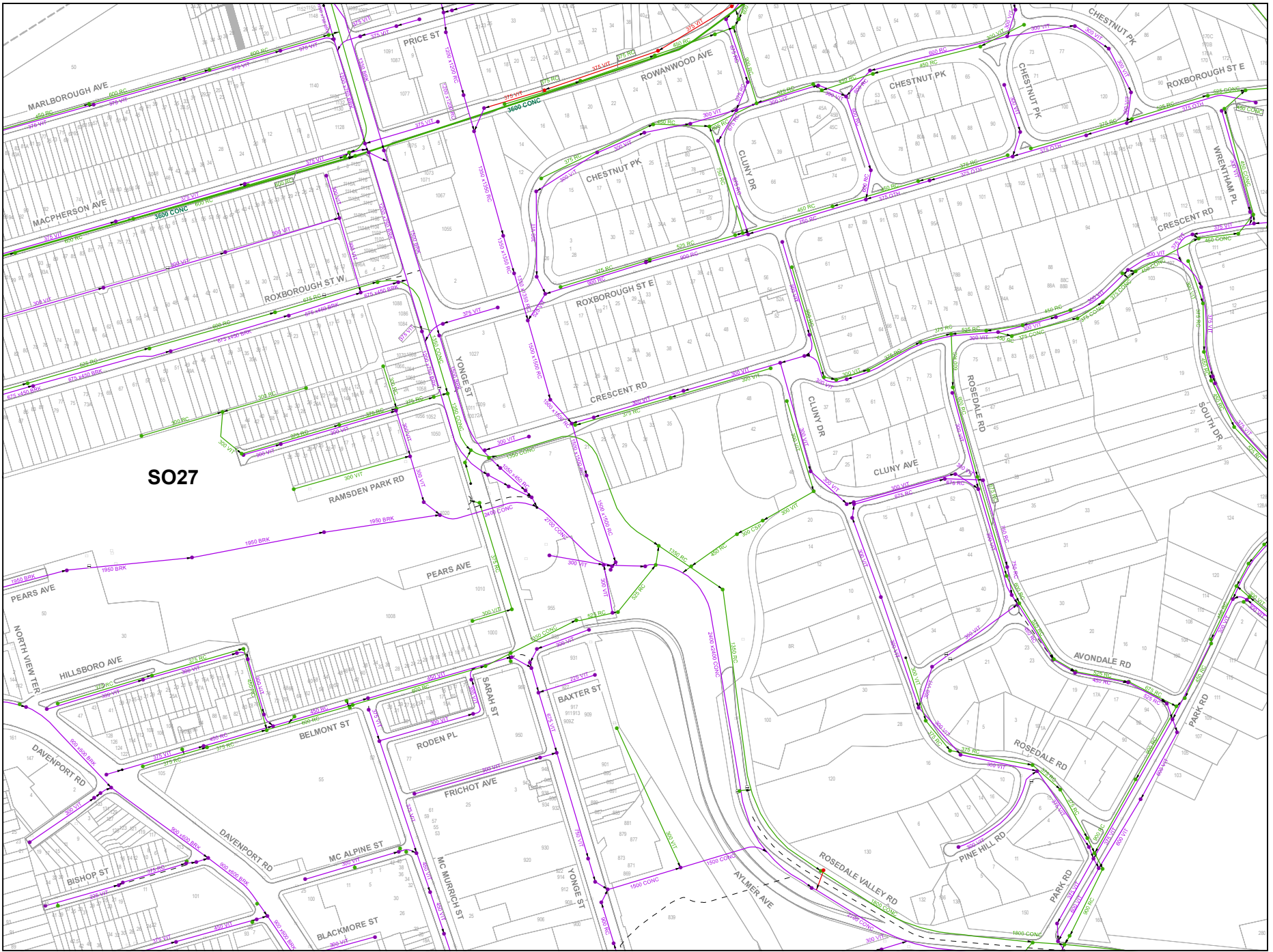
- |   |  |
|---|--|
| <ul style="list-style-type: none"> <li>Storm</li> <li>Sanitary Trunk</li> <li>Storm Trunk</li> <li>Abandoned Sewer</li> </ul> | <ul style="list-style-type: none"> <li>River</li> <li>Highway</li> <li>Curb</li> <li>Wards Boundary</li> </ul> |
|---|--|
- Third Edition  
Date: 01/09/2010
- 0 50 100 150 200 Metres

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580	612	646
581	613	647
582	614	648



**Toronto Sewer Atlas**

<ul style="list-style-type: none"> <li>Large Chamber</li> <li>Manhole           <ul style="list-style-type: none"> <li>Combined</li> <li>Dual</li> <li>Sanitary</li> <li>Storm</li> <li>Foundation</li> </ul> </li> </ul>	<ul style="list-style-type: none"> <li>Control Manhole           <ul style="list-style-type: none"> <li>Combined</li> <li>Dual</li> <li>Sanitary</li> <li>Storm</li> </ul> </li> </ul>	<ul style="list-style-type: none"> <li>Outfall</li> <li>Sewer Pump Station</li> <li>Sewer Pump Station</li> <li>Catchbasin           <ul style="list-style-type: none"> <li>Other</li> <li>Twin Inlet Catchbasin</li> </ul> </li> </ul>	<ul style="list-style-type: none"> <li>Sewer           <ul style="list-style-type: none"> <li>Foundation Drain</li> <li>Combined</li> <li>Sanitary</li> <li>Abandoned Sewer</li> </ul> </li> </ul>	<ul style="list-style-type: none"> <li>Storm</li> <li>Combined Trunk</li> <li>Sanitary Trunk</li> <li>Storm Trunk</li> </ul>	<ul style="list-style-type: none"> <li>River</li> <li>Highway</li> <li>Curb</li> <li>Wards Boundary</li> </ul>
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Third Edition  
Date: 01/09/2010

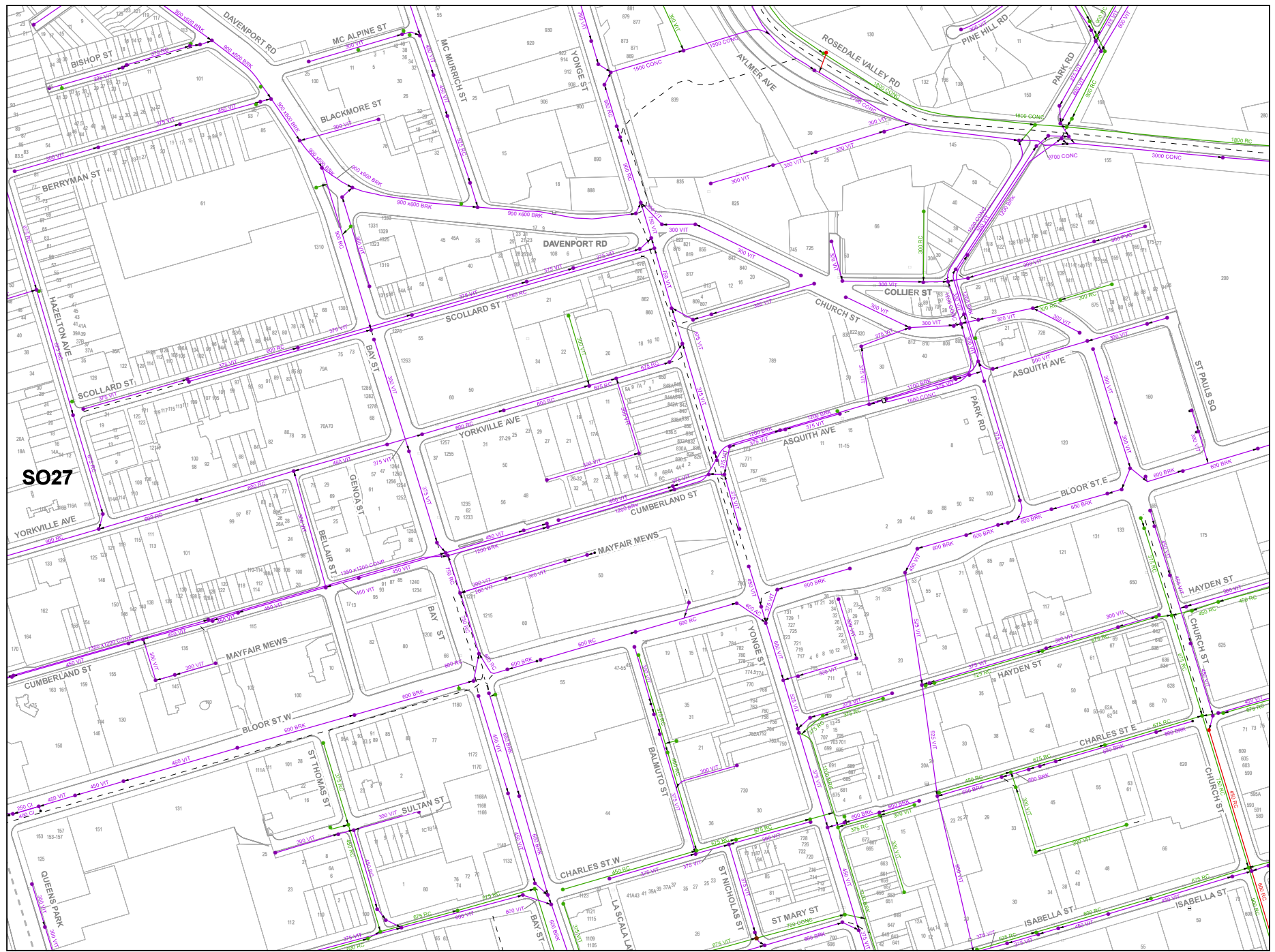


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612	646	681
613	647	682
614	648	683





**Toronto Sewer Atlas**

Large Chamber	Control Manhole	Outfall	Sewer	Storm	River
Manhole	Dual	Sewer Pump Station	Foundation Drain	Combined Trunk	Highway
Combined	Sanitary	Sewer Pump Station	Combined	Sanitary Trunk	Curb
Dual	Storm	Catchbasin	Sanitary	Storm Trunk	Wards Boundary
Sanitary	Other	Twin Inlet Catchbasin	Abandoned Sewer	River	
Storm					
Foundation					

Third Edition  
Date: 01/09/2010



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613	647	682
614	648	683
615	649	684

TORONTO SEWER SYSTEM STUDY AREA 8

SOUTH CALCULATION AREA

145 CIRCULAR 2.44/2.44 INFLOW 144 4389 OUTFLOW 146 B.NO. 67270 EXIST.COMB. 145  
YU 94.069 YL 93.609 QF 23963 DQ 23 QDLM 350 VNIGHT1.09 DUC -0.57 DLC -0.58 QLM 20959 CAP 3004  
SU 99.119 SL 99.296 AF 4.668 DQD 0.2 HDLM 0.20 HNIGHT0.07 DUS -3.18 DLS -3.83 RAIN 8MS2 QLM/QF 0.87  
RES 234 A 0.08 VF 5.13 GAMMA 1.00 VDLM 1.95 VNORM 0.0 HUM 1.87 HLM 1.86 QRQLM 20460 DY 0.46  
IW 0.0 L 53.3 S 1/116 N 0.0130 SCOD 112 DWB 0.0 YUM 95.94 YLM 95.47 VLM 5.52 DH 0.01

4355 CIRCULAR 0.61/0.61 INFLOW 4354 OUTFLOW 4356 B.NO. 86700 EXIST.COMB. 4355  
YU 112.546 YL 112.302 QF 388 DQ 219 QDLM 1 VNIGHT0.21 DUC -0.00 DLC 0.15 QLM 379 CAP 9  
SU 116.130 SL 116.048 AF 0.292 DQD 0.4 HDLM 0.02 HNIGHT0.00 DUS -2.98 DLS -2.98 RAIN 8MS2 QLM/QF 0.98  
RES 44 A 0.82 VF 1.33 GAMMA 0.93 VDLM 0.30 VNORM 0.0 HUM 0.61 HLM 0.76 QRQLM 378 DY 0.24  
IW 0.0 L 66.4 S 1/272 N 0.0130 SCOD 004 DWB 0.0 YUM 113.15 YLM 113.06 VLM 1.42 DH -0.15

4356 CIRCULAR 0.69/0.69 INFLOW 4355 OUTFLOW 4357 B.NO. 86700 EXIST.COMB. 4356  
YU 112.238 YL 112.165 QF 532 DQ 0 QDLM 1 VNIGHT0.22 DUC 0.14 DLC 0.18 QLM 366 CAP 165  
SU 116.048 SL 116.142 AF 0.373 DQD 0.0 HDLM 0.02 HNIGHT0.00 DUS -2.98 DLS -3.10 RAIN 8MS2 QLM/QF 0.69  
RES 44 A 0.0 VF 1.42 GAMMA 0.93 VDLM 0.30 VNORM 0.0 HUM 0.83 HLM 0.87 QRQLM 366 DY 0.07  
IW 0.0 L 20.4 S 1/280 N 0.0130 SCOD 004 DWB 0.0 YUM 113.06 YLM 113.04 VLM 1.43 DH -0.05

4357 CIRCULAR 0.69/0.69 INFLOW 4356 OUTFLOW 4358 B.NO. 86700 EXIST.COMB. 4357  
YU 112.147 YL 111.958 QF 596 DQ 144 QDLM 1 VNIGHT0.25 DUC 0.20 DLC 0.32 QLM 479 CAP 117



SU 116.142 SL 116.155 AF 0.373 DQD 0.3 HDLM 0.02 HNIGHT0.00 DUS -3.10 DLS -3.18 RAIN 8MS2 QLM/QF 0.80  
 RES 44 A 0.54 VF 1.60 GAMMA 0.93 VDLM 0.35 VNORM 0.0 HUM 0.89 HLM 1.01 QRQLM 478 DY 0.19  
 IW 0.0 L 42.1 S 1/223 N 0.0130 SCOD 004 DWB 0.0 YUM 113.04 YLM 112.97 VLM 1.65 DH -0.12  
 4358 CIRCULAR 0.69/0.69 INFLOW 4357           OUTFLOW 4360       B.NO. 86700           EXIST. COMB. 4358  
 YU 111.918 YL 111.830 QF 669 DQ 0 QDLM 1 VNIGHT0.28 DUC 0.36 DLC 0.42 QLM 469 CAP 200  
 SU 116.155 SL 116.249 AF 0.373 DQD 0.0 HDLM 0.02 HNIGHT0.00 DUS -3.18 DLS -3.31 RAIN 8MS2 QLM/QF 0.70  
 RES 44 A 0.0 VF 1.79 GAMMA 0.93 VDLM 0.38 VNORM 0.0 HUM 1.05 HLM 1.11 QRQLM 468 DY 0.09  
 IW 0.0 L 15.5 S 1/177 N 0.0130 SCOD 004 DWB 0.0 YUM 112.97 YLM 112.94 VLM 1.35 DH -0.06  
 4359 CIRCULAR 0.38/0.38 INFLOW            - OUTFLOW 4360       B.NO. 85630           EXIST. COMB. 4359  
 YU 112.707 YL 112.079 QF 160 DQ 130 QDLM 0 VNIGHT0.22 DUC -0.07 DLC 0.51 QLM 111 CAP 49  
 SU 116.109 SL 116.249 AF 0.113 DQD 0.2 HDLM 0.01 HNIGHT0.00 DUS -3.10 DLS -3.28 RAIN 8MS2 QLM/QF 0.69  
 RES 32 A 0.45 VF 1.41 GAMMA 1.00 VDLM 0.25 VNORM 0.0 HUM 0.31 HLM 0.89 QRQLM 111 DY 0.63  
 IW 0.0 L 80.5 S 1/128 N 0.0130 SCOD 004 DWB 0.0 YUM 113.01 YLM 112.97 VLM 1.29 DH -0.59  
 4360 CIRCULAR 0.69/0.69 INFLOW 4359 4358    OUTFLOW 4361       B.NO. 85640           EXIST. COMB. 4360  
 YU 111.772 YL 111.689 QF 489 DQ 0 QDLM 1 VNIGHT0.20 DUC 0.45 DLC 0.45 QLM 568 CAP -78  
 SU 116.249 SL 116.219 AF 0.373 DQD 0.0 HDLM 0.02 HNIGHT0.01 DUS -3.34 DLS -3.39 RAIN 8MS2 QLM/QF 1.16  
 RES 32 A 0.0 VF 1.31 GAMMA 1.00 VDLM 0.31 VNORM 0.0 HUM 1.14 HLM 1.14 QRQLM 567 DY 0.08  
 IW 0.0 L 27.4 S 1/330 N 0.0130 SCOD 004 DWB 0.0 YUM 112.91 YLM 112.83 VLM 1.52 DH 0.00  
  
 4361 CIRCULAR 0.77/0.76 INFLOW 4360 5569    OUTFLOW 4368       B.NO. 85650           EXIST. COMB. 4361  
 YU 111.625 YL 111.345 QF 819 DQ 83 QDLM 1 VNIGHT0.28 DUC 0.44 DLC 0.60 QLM 635 CAP 184

SU 116.219 SL 115.725 AF 0.453 DQD 0.1 HDLM 0.02 HNIGHT0.00 DUS -3.39 DLS -3.02 RAIN 8MS2 QLM/QF 0.78  
RES 32 A 0.29 VF 1.81 GAMMA 1.00 VDLM 0.39 VNORM 0.0 HUM 1.20 HLM 1.36 QRQLM 634 DY 0.28  
IW 0.0 L 55.2 S 1/ 197 N 0.0130 SCOD 004 DWB 0.0 YUM 112.83 YLM 112.70 VLM 1.86 DH -0.15

4368 CIRCULAR 0.77/0.76 INFLOW 4367 4361 P106 OUTFLOW 4369 B.NO. 85660 EXIST. COMB. 4368  
YU 111.336 YL 110.187 QF 2329 DQ 0 QDLM 3 VNIGHT0.80 DUC 0.21 DLC 0.94 QLM 1397 CAP 931  
SU 115.725 SL 115.237 AF 0.453 DQD 0.0 HDLM 0.02 HNIGHT0.00 DUS -3.42 DLS -3.35 RAIN 8MS2 QLM/QF 0.60  
RES 32 A 0.0 VF 5.14 GAMMA 1.00 VDLM 1.04 VNORM 0.0 HUM 0.97 HLM 1.70 QRQLM 1393 DY 1.15  
IW 0.0 L 28.0 S 1/ 24 N 0.0130 SCOD 004 DWB 0.0 YUM 112.30 YLM 111.89 VLM 3.09 DH -0.74

4369 CIRCULAR 0.92/0.91 INFLOW 4368 4352 5539 OUTFLOW 4370 B.NO. 85670 EXIST. COMB. 4369  
YU 110.123 YL 109.409 QF 2203 DQ 53 QDLM 10 VNIGHT0.53 DUC 0.56 DLC 0.31 QLM 2572 CAP -368  
SU 115.237 SL 113.954 AF 0.649 DQD 0.1 HDLM 0.04 HNIGHT0.01 DUS -3.64 DLS -3.32 RAIN 8MS2 QLM/QF 1.17  
RES 32 A 0.19 VF 3.39 GAMMA 0.98 VDLM 0.94 VNORM 0.0 HUM 1.47 HLM 1.22 QRQLM 2562 DY 0.71  
IW 0.0 L 50.9 S 1/ 71 N 0.0130 SCOD 004 DWB 0.0 YUM 111.60 YLM 110.63 VLM 3.96 DH 0.25

4370 CIRCULAR 0.92/0.91 INFLOW 4369 OUTFLOW 4371 B.NO. 85670 EXIST. COMB. 4370  
YU 109.324 YL 108.867 QF 1982 DQ 149 QDLM 10 VNIGHT0.48 DUC 0.40 DLC 0.05 QLM 2683 CAP -699  
SU 113.954 SL 114.503 AF 0.649 DQD 0.2 HDLM 0.04 HNIGHT0.01 DUS -3.32 DLS -4.67 RAIN 8MS2 QLM/QF 1.35  
RES 32 A 0.53 VF 3.05 GAMMA 0.98 VDLM 0.88 VNORM 0.0 HUM 1.31 HLM 0.96 QRQLM 2673 DY 0.46  
IW 0.0 L 40.2 S 1/ 88 N 0.0130 SCOD 004 DWB 0.0 YUM 110.63 YLM 109.83 VLM 4.13 DH 0.35

4371 CIRCULAR 0.92/0.91 INFLOW 4370 OUTFLOW 4388 B.NO. 85670 EXIST. COMB. 4371  
YU 108.836 YL 108.721 QF 2052 DQ 0 QDLM 10 VNIGHT0.49 DUC 0.08 DLC 0.0 QLM 2683 CAP -630

SU 114.503 SL 114.463 AF 0.649 DQD 0.0 HDLM 0.04 HNIGHT0.01 DUS -4.67 DLS -4.83 RAIN 8MS2 QLM/QF 1.31  
 RES 32 A 0.0 VF 3.16 GAMMA 0.98 VDLM 0.90 VNORM 0.0 HUM 0.99 HLM 0.91 QRQLM 2673 DY 0.12  
 IW 0.0 L 9.4 S 1/ 82 N 0.0130 SCOD 004 DWB 0.0 YUM 109.83 YLM 109.63 VLM 4.13 DH 0.08  
 4388 CIRCULAR 1.53/1.52 INFLOW 4387 4371 OUTFLOW 4389 B.NO. 85670 EXIST. COMB. 4388  
 YU 108.623 YL 106.590 QF 13944 DQ 127 QDLM 16 VNIGHT1.20 DUC -0.99 DLC -0.99 QLM 3704 CAP 10240  
 SU 114.463 SL 110.967 AF 1.812 DQD 0.1 HDLM 0.04 HNIGHT0.01 DUS -5.31 DLS -3.85 RAIN 8MS2 QLM/QF 0.27  
 RES 19 A 0.44 VF 7.70 GAMMA 0.98 VDLM 1.44 VNORM 0.0 HUM 0.53 HLM 0.53 QRQLM 3688 DY 2.03  
 IW 0.0 L 55.8 S 1/ 27 N 0.0130 SCOD 008 DWB 0.0 YUM 109.15 YLM 107.12 VLM 6.56 DH 0.01  
 4389 CIRCULAR 1.53/1.52 INFLOW 4388 OUTFLOW 145 B.NO. 85670 EXIST. COMB. 4389  
 YU 95.526 YL 94.886 QF 7136 DQ 51 QDLM 16 VNIGHT0.61 DUC -0.33 DLC 0.20 QLM 3733 CAP 3403  
 SU 110.967 SL 99.119 AF 1.812 DQD 0.0 HDLM 0.05 HNIGHT0.01 DUS -14.25 DLS -2.51 RAIN 8MS2 QLM/QF 0.52  
 RES 19 A 0.18 VF 3.94 GAMMA 0.98 VDLM 0.90 VNORM 0.0 HUM 1.19 HLM 1.72 QRQLM 3717 DY 0.64  
 IW 0.0 L 67.1 S 1/ 105 N 0.0130 SCOD 009 DWB 0.0 YUM 96.71 YLM 96.61 VLM 3.97 DH -0.53

Contractions used in HVM output...

1st line: pipe number, cross-section, pipe size...width/height(m), inflow and outflow pipes, block number, sewer type, pipe no.

2nd line: YU, YL = upper and lower invert elevations (m)

QF = full flow capacity (L/sec)

DQ = maximum storm runoff from tributary area (L/sec)

QDLM = peak DWF at lower end (L/sec)

VNIGHT = night DWF velocity (m/sec)

DUC, DLC = difference between maximum HGL elevation and section crown elevation at upper and lower ends (m)

(-ve means partial fill)

QLM = maximum flow rate at lower end (L/sec) under a 2yr storm

CAP = free capacity at lower end when loaded by QLM

3rd line: SU, SL = upper and lower surface elevations (m)

AF = cross-sectional area (m<sup>2</sup>)

DQD = DWF from tributary area (L/sec)

HDLM = flow depth corresponding to QDLM (m)

HNIGHT = night DWF depth (m)

RAIN = storm corresponding to QLM... 8MS2 = 8th Study Area, 2yr model storm

QLM/QF = ratio of maximum flow rate at lower end to full-flow capacity

4th line: RES = population density (residents/ha)

A = tributary area (ha)

VF = flow velocity corresponding to QF (m/sec)

GAMMA = imperviousness ratio

VDLM = flow velocity corresponding to QDLM (m/sec)

VNORM = normal flow velocity for QDLM (m/sec)

HUM, HLM = maximum flow depths above invert at upper and lower ends

QRQLM = portion of storm flow within QLM (L/sec)

DY = difference between upper and lower invert elevations (m)

5th line: IW = industrial/large water inflow (L/sec)

L = segment length (m)

S = slope of pipe

N = Manning's n

SCOD = surface code of tributary area

DWB = backwater build-up under QDLM (m)

YUM, YLM = maximum HGL elevations at upper and lower ends

VLM = flow velocity corresponding to QLM (m/sec)

DH = indicator whether HGL is steeper or flatter than pipe slope

= (YUM-YLM) - DY